# Polymers for Space Applications Processed by Plasma Immersion Ion Implantation

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### Protection of Components for Spacecrafts Orbiting LEO

Low Earth Orbit (LEO) environment (180-650 km) : rich in atomic oxygen, degrades polymeric materials (like Kapton, Mylar or Teflon) used in satellites.

May erode certain polymers by over 2 µm in 90 days

Oxygen resistant polymers could improve the lifetime of satellites and space stations and could find many applications in space, including huge fold-up antennas, inflatable mirrors & lenses, solar sails...

Kapton is extensively used in thermal blankets



International Space Station orbiting LEO region (~ 450 km)

**Oxidation protection:** Thin layers of several metal oxides such as  $Al_2O_3$ , MgO, or SiO<sub>2</sub> are being studied as protective coatings for polymers in LEO

**Thermal transients** (-100° C to +100 ° C) : Superior adhesion of the thin film is required  $\emptyset$  **Plasma Immersion Ion Implantation and Deposition (PIII)** of metal ions is ideal.

**PIII in polymers**: charging of the dielectric is proportional to plasma density

Typically for ~ 20  $\mu$ m thick polymers: n ~ 10<sup>17</sup> m<sup>-3</sup> Ø  $\Delta$ V ~ 7kV in 2 $\mu$ s n ~ 10<sup>15</sup> m<sup>-3</sup> Ø  $\Delta$ V ~ 700V in 60 $\mu$ s

# In metal plasmas generated by vacuum arcs: Magnetic field increases plasma density by two orders of magnitude



# Objectives

# Aluminum implantation in Kapton® by three different methods

- Direct implantation in a magnetized AI plasma
- Direct implantation in an unmagnetized AI plasma
- Al deposition + implantation in nitrogen plasma (recoil implantation)

#### **Resistance tests for space environment**

- Oxygen degradation (oxygen plasmas)
- Thermal cycling
- Adhesion test

# **Direct Aluminum implantation**

#### **Experimental Set-up**



Vacuum Arc:Al cathodeTungsten grid anodeHV trigger : 10-13 kV

Vacuum chamber $\phi$ =0.22m, L=1.05mBase pressure $\sim$  1x10-4 PaB field : 150G-7kG

Sample holder: 85cm from cathode

Straight magnetic filter: not so good filtering but good plasma transport. Macroparticles avoided and deposition minimized by orienting samples parallel to plasma stream

#### **Implantation Conditions**





#### With B = 125 G larc = 1kA 7μs pulses, 2.5 kV, 900 Hz (13-14 pulses / discharge) 100 discharges

With B = 0 larc = 1 kA 7µs pulses, 6 kV, 900 Hz 800 discharges

## **Recoil Aluminum implantation**



**200 Å, 500 Å and 2000 Å aluminum films deposited** by electron beam on Kapton samples followed by

**Implantation** in **Nitrogen** (n ~  $10^{10}$  cm<sup>-3</sup>, T<sub>e</sub> < 10 eV) and argon plasmas.

**HV pulses:** 5 μs, 100Hz, 5 kV

Treatment time of 30 minutes

## Analysis

#### **Elemental composition and morphology**

- ➢ RBS
- > XPS

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➢ SEM , EDS

#### Oxygen degradation

Oxygen plasma: 40kHz parallel plate capacitive reactor

200 mTorr, 200W ( $10^{10}$  cm<sup>-3</sup>, 1-2 eV), ~ one hour exposure

Transmittance and Reflectance (Hitachi U-3501 spectrophotometer)

#### Thermal cycling

- 1 minute liquid nitrogen immersion (-196 °C)
- > 1 minute pre-heated oven (100 °C)
- > 15 cycles

#### **Adhesion Test**

applying and removing a pressure sensitive tape + SEM

### Results

#### **Oxygen Degradation**



### **Direct Implantation in Magnetized Plasmas**

**RBS** Æ retained doses of 10<sup>16</sup> atoms/cm<sup>2</sup>, but mostly at the surface





# SEM : morphology conserved after oxygen degradation, thermal cycling and adhesion tests





**Pristine Kapton** 

After tests

# Without treatment, after oxygen exposure





#### **Total reflectance increases**



## **Direct Implantation in Unmagnetized Plasmas**

- Treatment time increased eightfold was not enough to compensate the plasma density decreased by two orders of magnitude without magnetic field. This resulted in lack of uniformity
- Treated samples had "good" and "bad" parts.
- "Good" parts behaved in the same way as samples treated in magnetized plasmas: no oxygen degradation revealed by conserved transparency, and conserved morphology after oxygen exposure, thermal cycling and adhesion tests.
- "Bad" parts behaved like untreated samples: "carpet" like morphology after oxygen exposure, loss of transparency.

## **Deposition and recoil implantation**

For 200 Å and 500 Å depositions (but not for 2000 Å films), nitrogen and argon implantation results in a cracked film.





- Cracking of the deposited film is not caused by differences in thermal expansion since it does not occur after oven heating at 100 °C or even at 200 °C.
- Immersion of the deposited samples in nitrogen or argon plasmas does not result in cracking, which occurs as soon as the high voltage pulses are turned on.
- In direct implantation process, an aluminum film is also deposited without cracking, probably due to ion induced stress relief.
- Cracking in recoil implantation could be related to the formation of a stressed aluminum nitride (with nitrogen plasmas) and a stressed aluminum dioxide (which occurs in argon plasmas, even with very low oxygen contamination) films, although ion induced stress relief would be expected in this case as well.
- We have no conclusive explanation for the observed ion induced cracking.

## Conclusions

- Kapton samples implanted with AI in a magnetized vacuum arc discharge resulted in excellent protection of the polymer against oxygen degradation.
- Retained doses of 10<sup>16</sup> atoms/cm<sup>2</sup> was obtained, and although most of the atoms are concentrated on the surface, an intermediate ion mixing layer was formed.
- Adhesion test after thermal cycling shows good adhesion to the substrate.
- Implantation with AI in unmagnetized plasmas produces a protection layer as effective as in the magnetized case, but needs much longer treatment times, incompatible with present machine configuration.
- Al deposition by e-beam, followed by recoil implantation in nitrogen and argon plasmas resulted in a cracked film, induced by ion bombardment. No conclusive explanation has been found for this observation.