



Ciclo de Palestras Sobre Controle Térmico de Satélites

Radiadores Espaciais

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Divisão de Mecânica Espacial e Controle - DMC

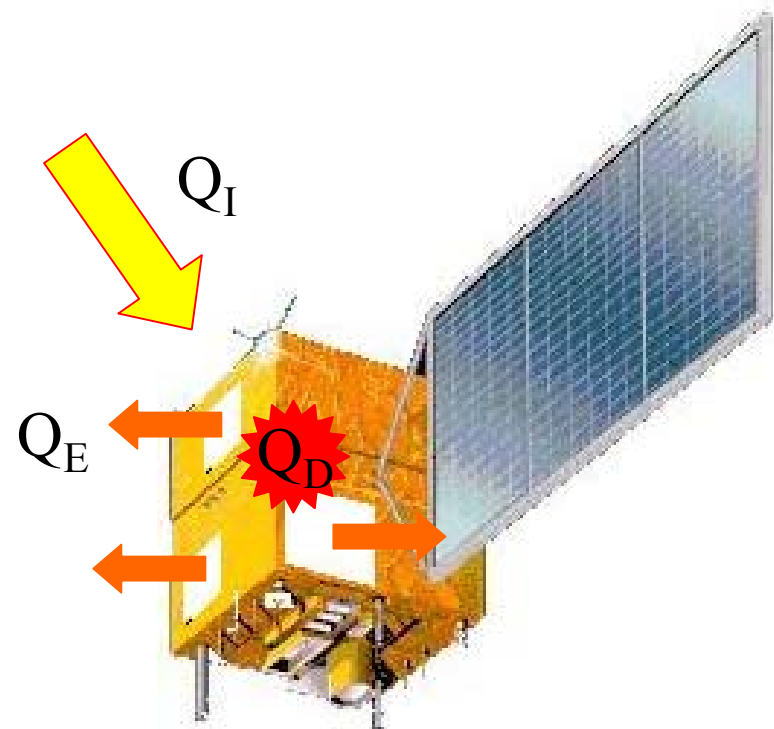
Balanco Térmico Global no Satélite

$$\epsilon A_{\text{eff}} \sigma T_S^4 = \alpha A_{\text{eff}} Q_I + Q_D$$

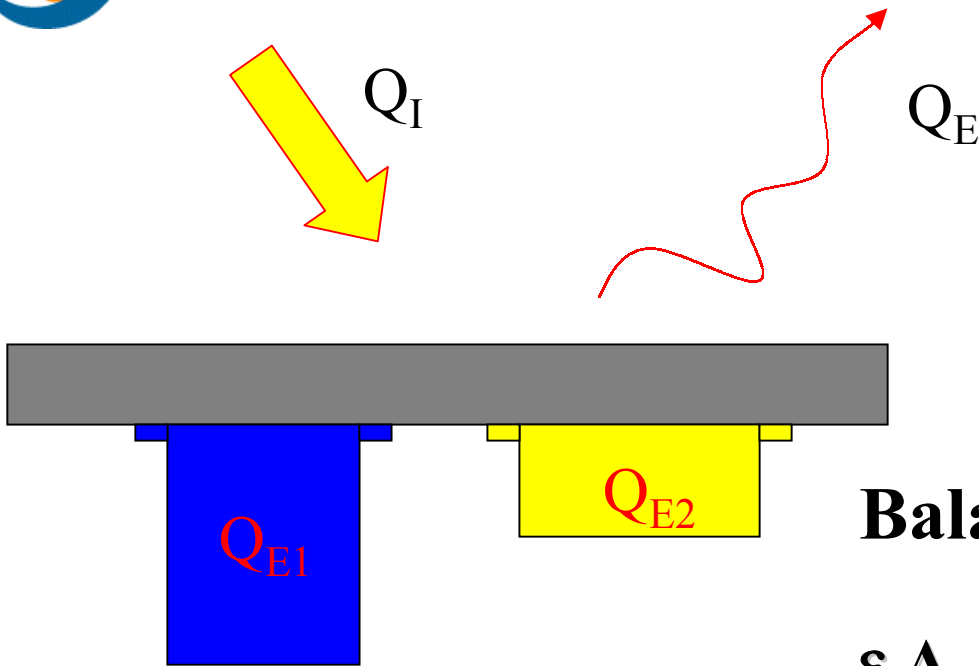
**Calor emitido
pelo satélite**

**Calor externo
absorvido pelo
satélite**

**Calor dissipado
internamente
ao satélite**



⇒ O Calor excedente em um satélite é rejeitado para o espaço por meio de radiadores.

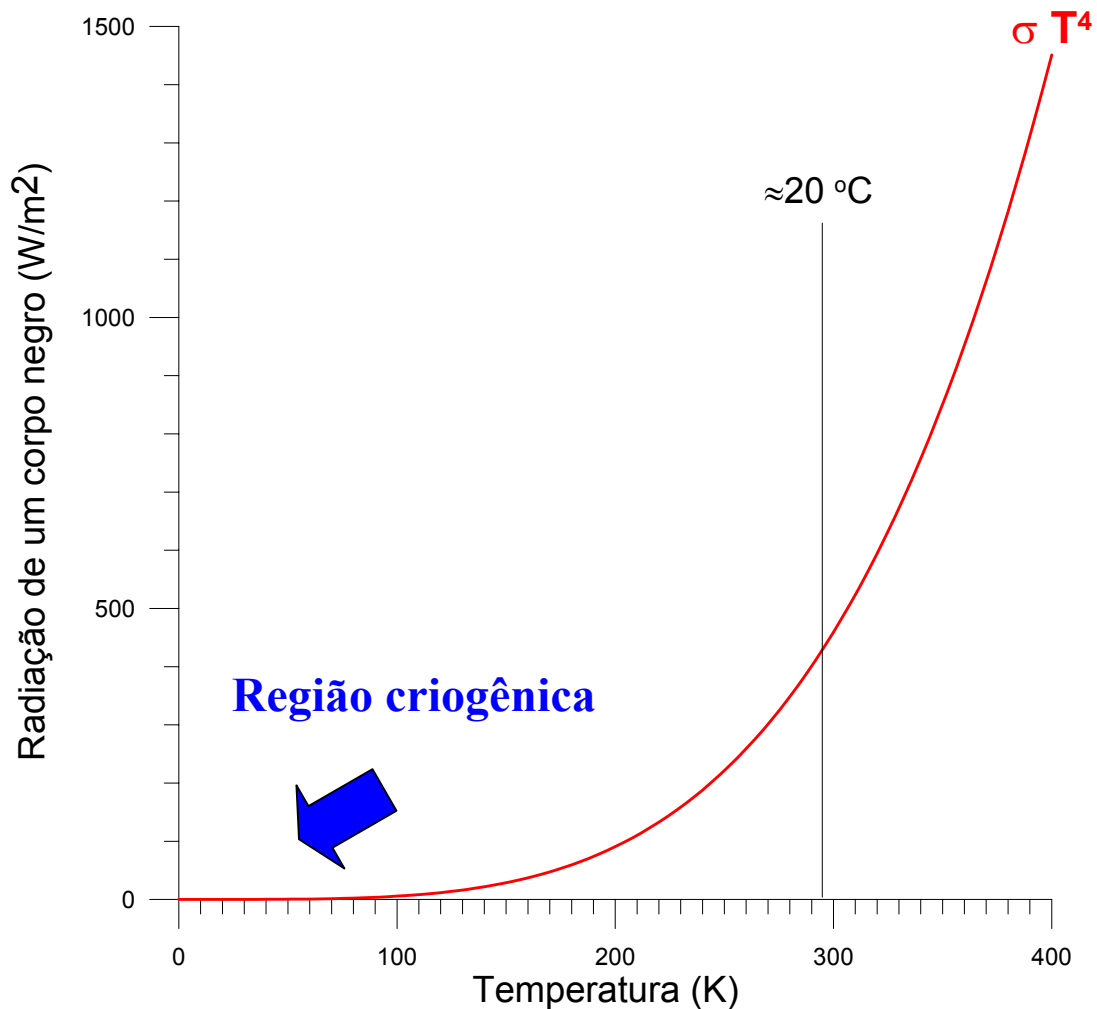


Balanço Térmico no Radiador

$$\varepsilon A_{\text{rad}} \sigma T_{\text{rad}}^4 = \alpha A_{\text{rad}} Q_I + Q_{E1+E2}$$

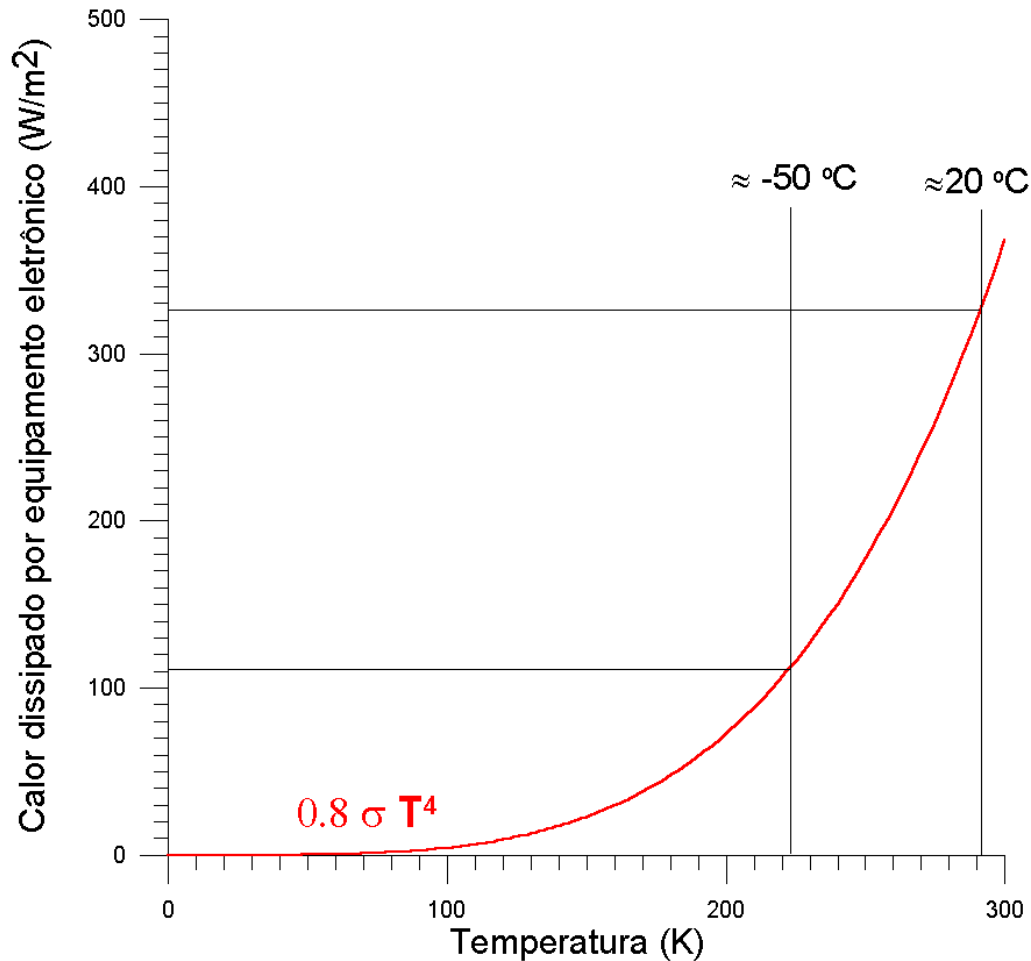
- Radiadores apresentam geralmente uma baixa relação α/ε .
- Em geral $\alpha < 0,2$ e $\varepsilon > 0,8$.

- A quantidade de calor emitida por um radiador é fortemente dependente da temperatura do mesmo: $\epsilon A_{\text{rad}} \sigma T_{\text{rad}}^4$



$$\sigma = 5,669 \cdot 10^{-8} \text{ W/m}^2 \text{ K}^4$$

- Tipicamente os radiadores rejeitam de 110 a 325 W/m² de calor dissipado pelos equipamentos eletrônicos.



- A temperatura máxima e mínima de operação do radiador não pode comprometer os requisitos de temperatura dos equipamentos à ele acoplados.
- Tipicamente opera-se no intervalo $5 \leq T_{\text{rad}} \leq 40 \text{ }^\circ\text{C}$.
- Radiadores criogênicos operam a temperaturas bem abaixo do intervalo acima (ver apresentação do Valeri a seguir).

Radiadores Espaciais

Classificação por
estrutura física

Classificação por
propriedade termo-óptica

Como parte
da estrutura
do satélite

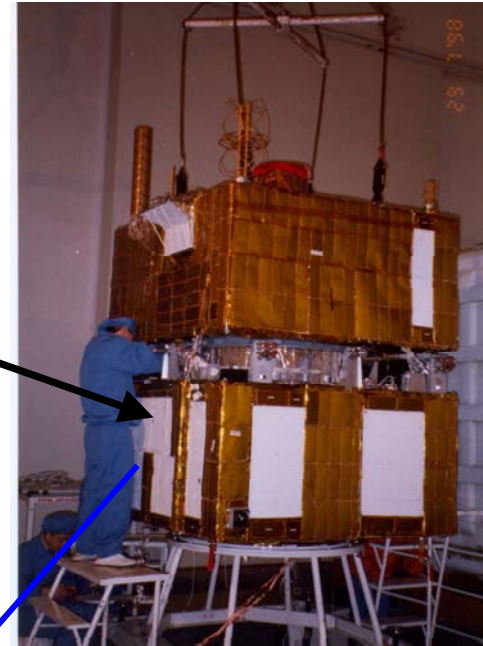
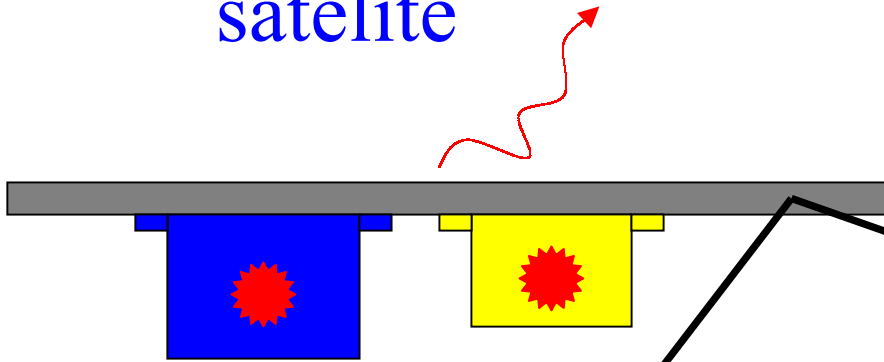
Fixado à
estrutura

Retrátil

Propriedades
termo-ópticas
constantes

Propriedades
termo-ópticas
variáveis

→ Radiador é parte integrante da estrutura do satélite



CBERS - FM1



SACI-1



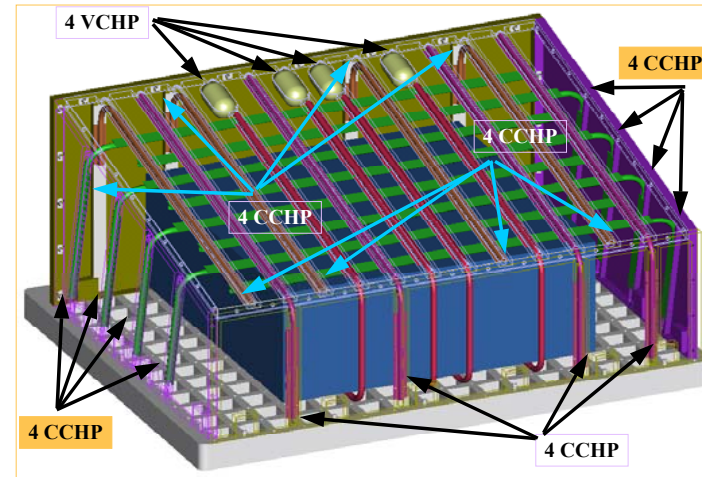
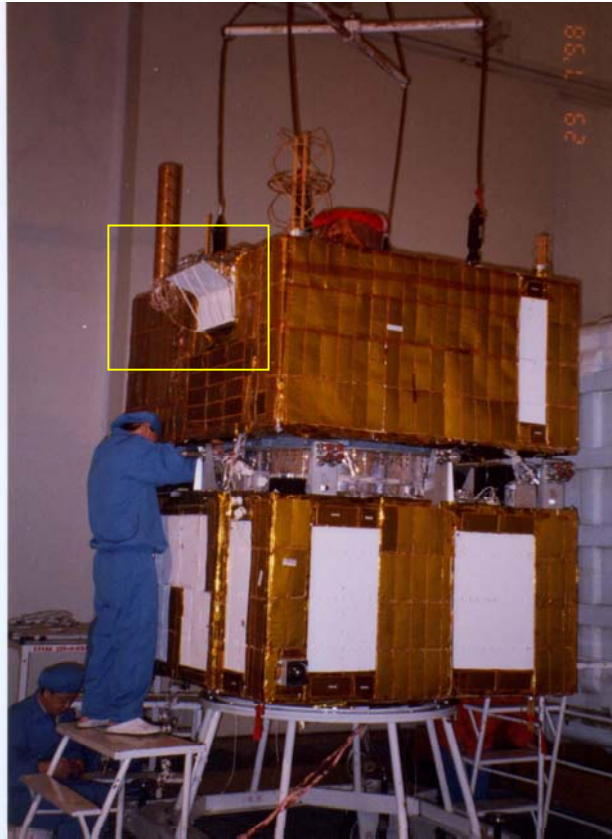
Painel das baterias



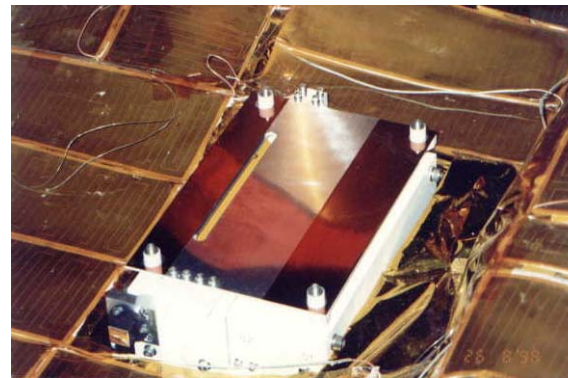
Painel BDR/Shunt
com HPs imbutidos

→ Fixado à estrutura

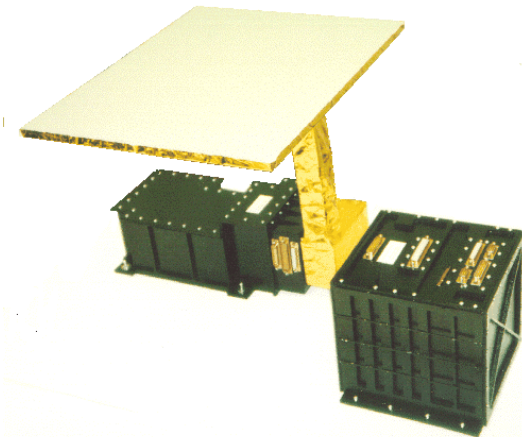
CBERS - FM1



Radiador do ExPS



Radiador do WFI
 CBERS - FM1

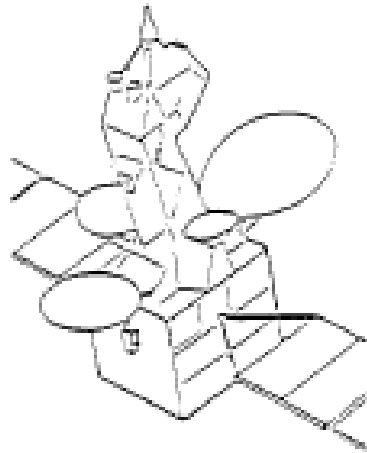


Radiador da CCD
 do FUSE

→ Radiadores Retráteis

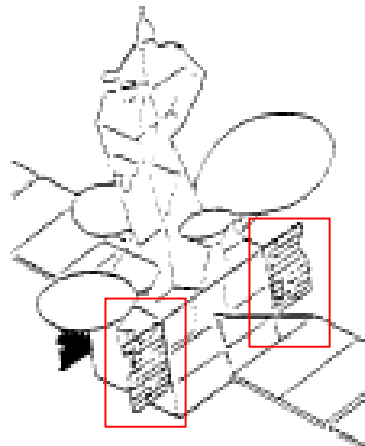
- Radiadores retráteis surgem da necessidade de um aumento significativo da área de rejeição de calor.

Nominal configuration

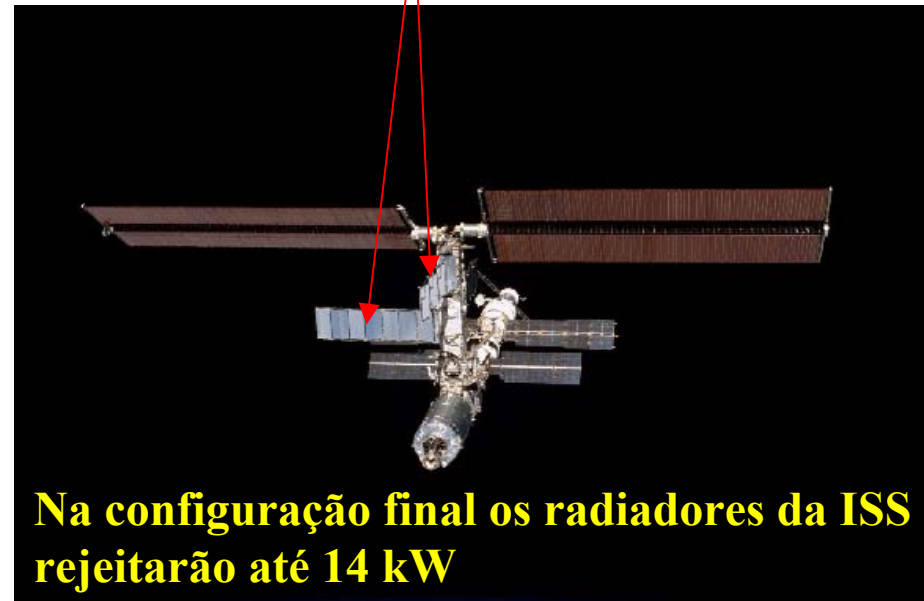
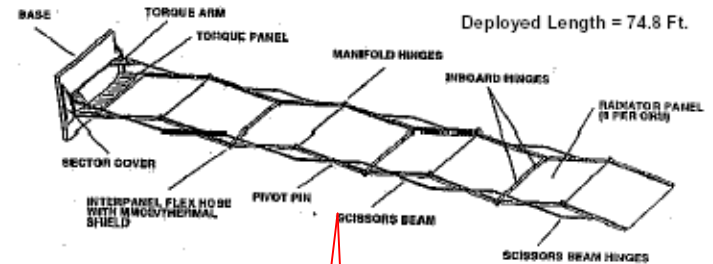


Rejected power : 800 W
 Temperature : $0^{\circ}\text{C} \leq T \leq 40^{\circ}\text{C}$
 Heat flux = 1.0 W/cm^2

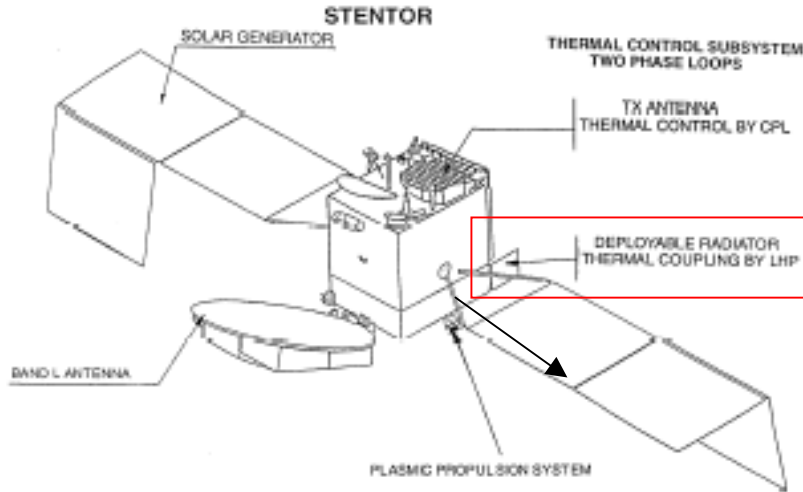
Nominal configuration
 + 4 deployable panels
 1.2 x 0.8 m
 one radiative face



Rejected power : 1600 W
 Temperature : $0^{\circ}\text{C} \leq T \leq 40^{\circ}\text{C}$
 Heat flux = 2.0 W/cm^2



Satellite de Télécommunications pour
 Expérimenter les Nouvelles
 Technologies en Orbite

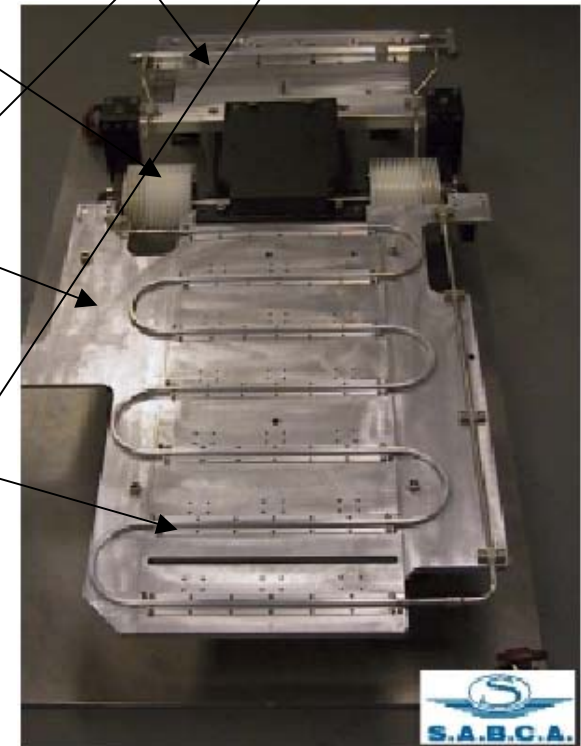
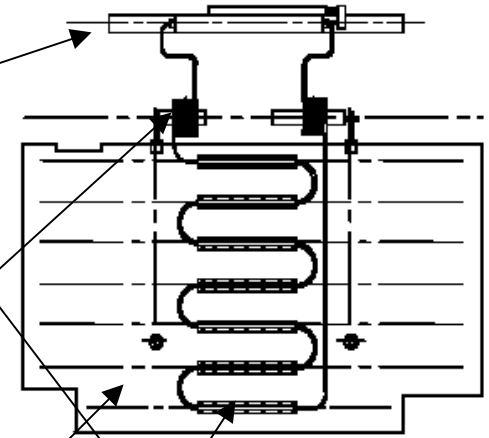


Evaporador do LHP

Linhas flexíveis
 helicoidais

Radiador com HPs
 imbutidos

Condensador do
 LHP



- one LHP (no redundancy)
- evaporator heat load ranging from 150 to 600 watts
- qualification temperature up to +85°C at the evaporator heat input interface
- static head of 2 m
- heat flux density up to 4 W/cm²
- « turnkey » start-ups with radiator panel temperatures as low as -50°C
- operational lifetime 15 years
- deployment capability from 90° to 180°
- mass 13 kg maximum

- Two LHPs (hot redundancy) tolerating single point failure ←
- Loop heat transfer capability up to 1200 watts ←
- Evaporator heat input interface qualification temperature up to +85°C
- Static head of 2 m
- Heat flux density up to 5 W/cm² ←
- Freeze-tolerant DR (condenser, isolator and radiator panel) ←
- Operational lifetime 15 years
- Deployment capability up to 180°

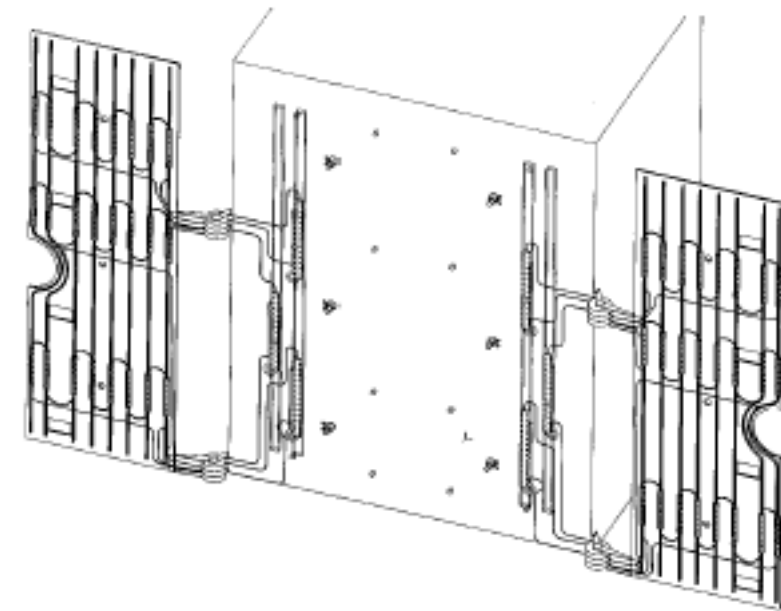


Figure 13 : 1300 W three-LHP DR derived from STENTOR baseline design

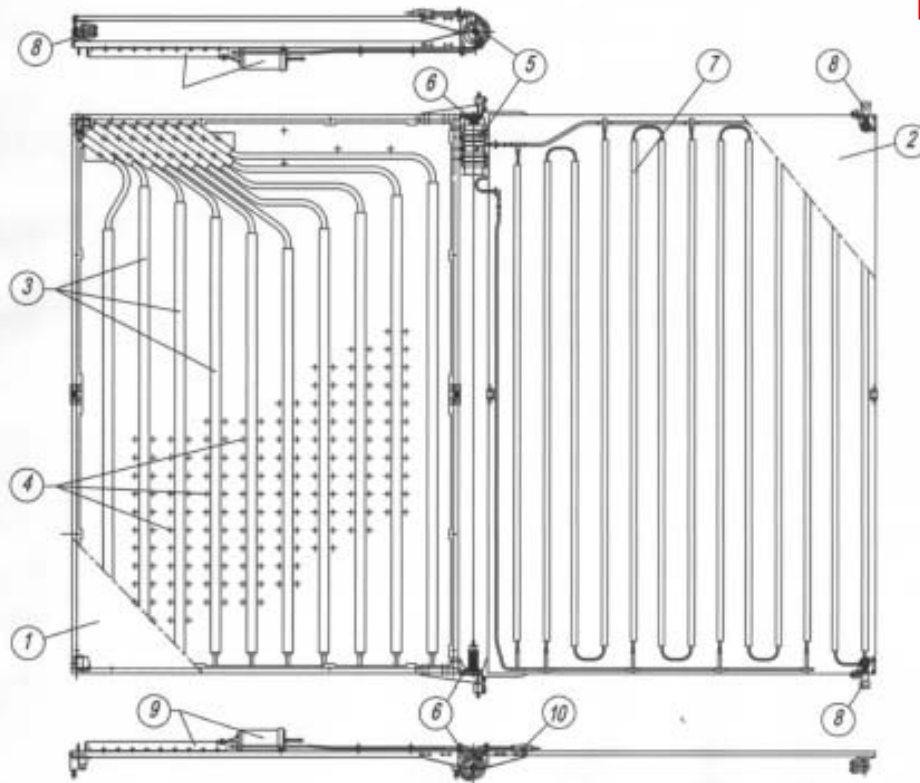
	STENTOR design	DELPHRAD design
Rejected heat (W)	380	400
DR Mass (kg)	13	9.5
Rejected heat / surface (W/m ²)	340	355
DR mass / rejected heat (kg/kW)	34	24

Radiadores Retráteis (cont.)

1500 W Deployable Radiator with Loop Heat Pipe

K. Goncharov, A. Orlov and A. Tarabrin
 Lavochkin Association

M. Gottero, V. Perotto, S. Tavera and G. P. Zoppo
 Alenia Spazio S.p.A.



- transferred heat power is from 10 to 1500 W;

- The heat input to the internal (fixed) panel is applied to eighth zones; the total area of the heaters does not exceed 1/10 of the panel area. The internal panel average temperature is from -20 to $+60$ [°C] at heat load of $10W \div 1500W$, correspondingly, and the heat sink temperature of 100 K;

- The thermal resistance of the LHP at maximum heat load ($Q_{max} = 1500W$) and maximum temperature of $+60^\circ C$ is less than 0.007 [K/W];

- The maximum thermal resistance of the whole Deployable Radiator under the same conditions is less than 0.013 (K/W) (temperature difference between contact surface of payload imitators and average temperature of radiating surface at heat power of $1500W$ is less than $20^\circ C$). Thermal resistance value includes AGHPS and LHP thermal resistance, thermal resistance of AGHP/LHP interface, thermal resistance of radiator sheet. In more details calculated and experimental values of thermal resistance are presented in paper [7].

Development of Loop Heat Pipe Deployable Radiator for Use on Engineering Test Satellite VIII (ETS-VIII)

Hiroaki Ishikawa, Akira Yao, Teturo Ogushi and Seiji Haga
 Mitsubishi Electric Corporation (MELCO)

Akihiro Miyasaka and Hiroyuki Noda
 National Space Development Agency of Japan (NASDA)

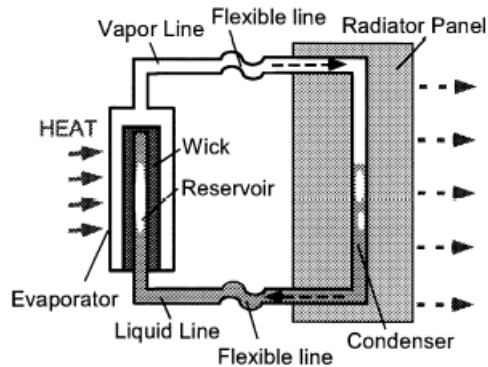
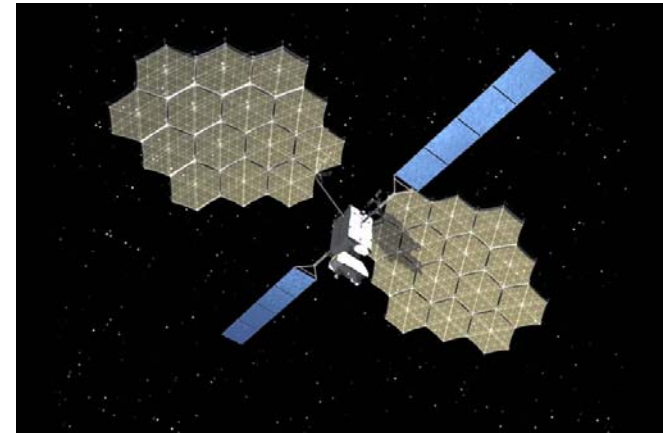


Figure 1 Schematic of Loop Heat Pipe(LHP)

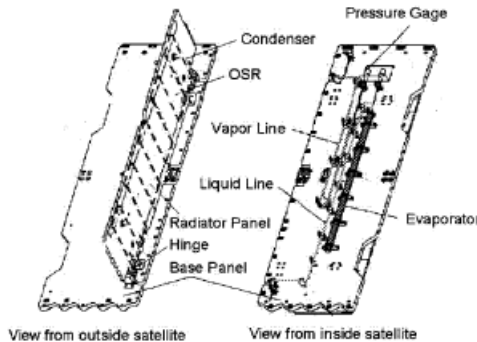
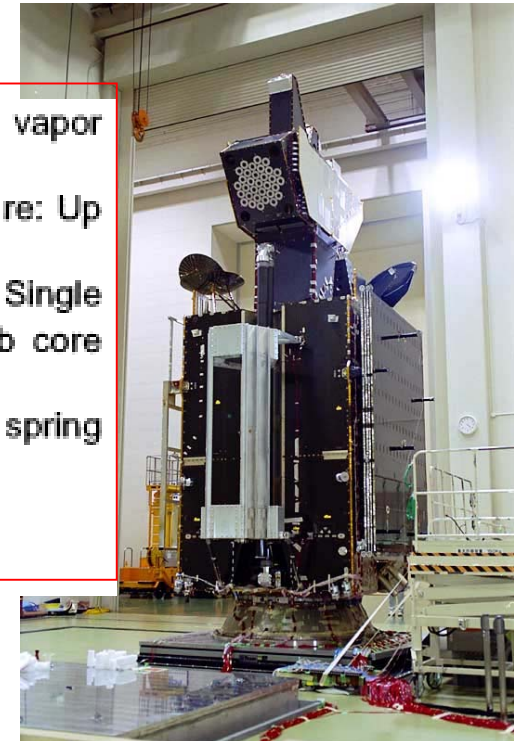


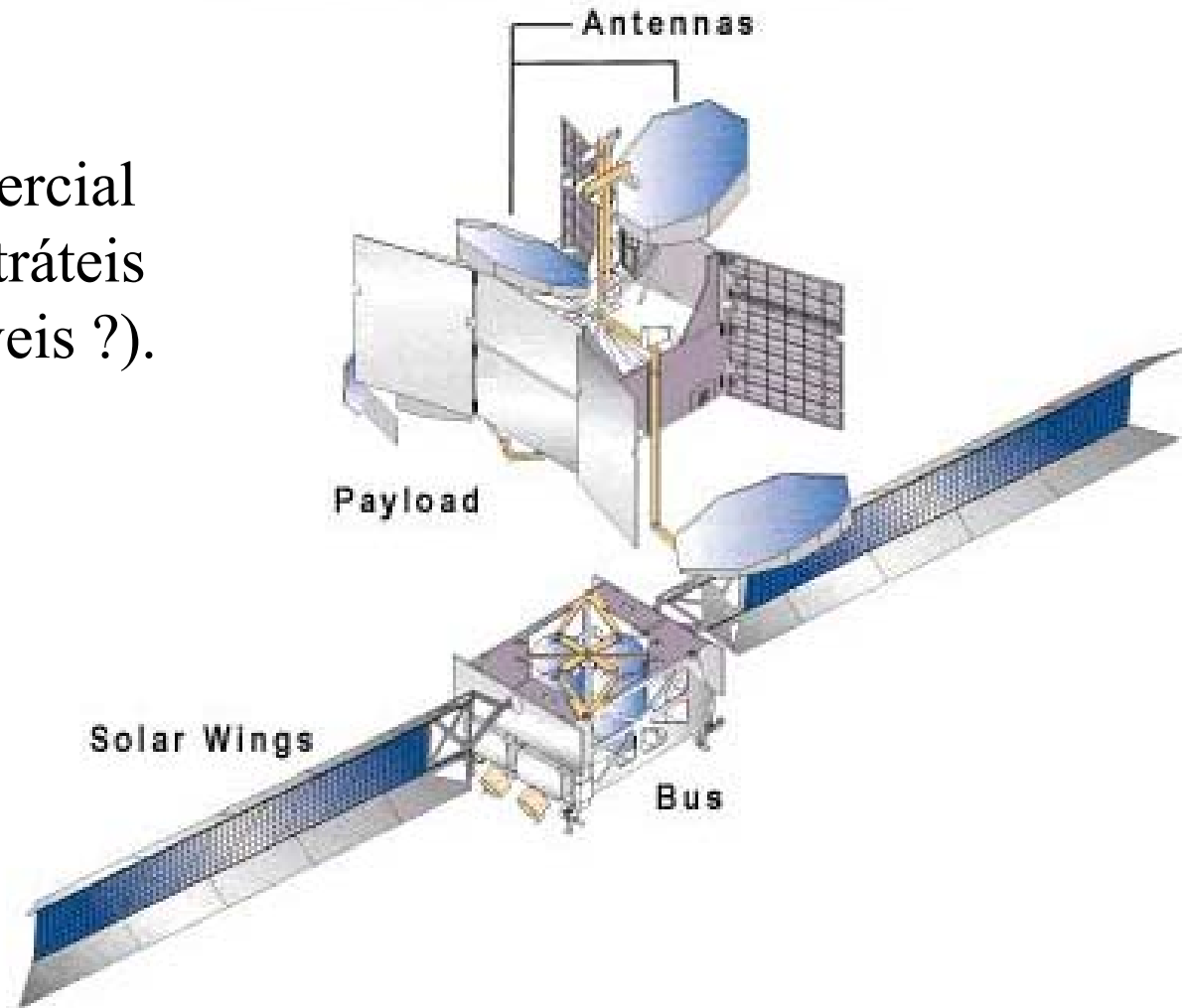
Figure 2 Schematic of Deployable Radiator for ETS-VIII

- *Evaporator heat load: Up to 1000watts (at vapor temperature -5~+65°C.
- *Evaporator Input interface qualification temperature: Up to +85°C
- *Radiator Panel: 1800×490mm Single panel, Single sided OSR coating, CFRP face-skin, Honeycomb core radiator panel
- *Heat rejection capability: Up to 400watts in spring equinox
- *Deployment Angle: 90°
- *Total Weight: 18.7kg

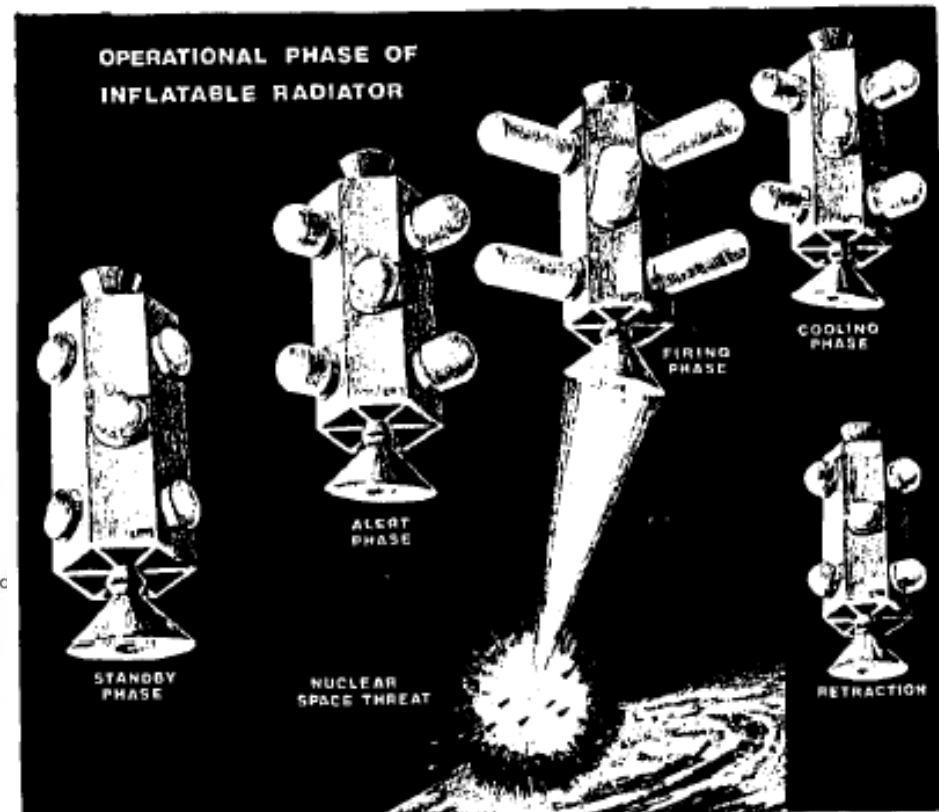
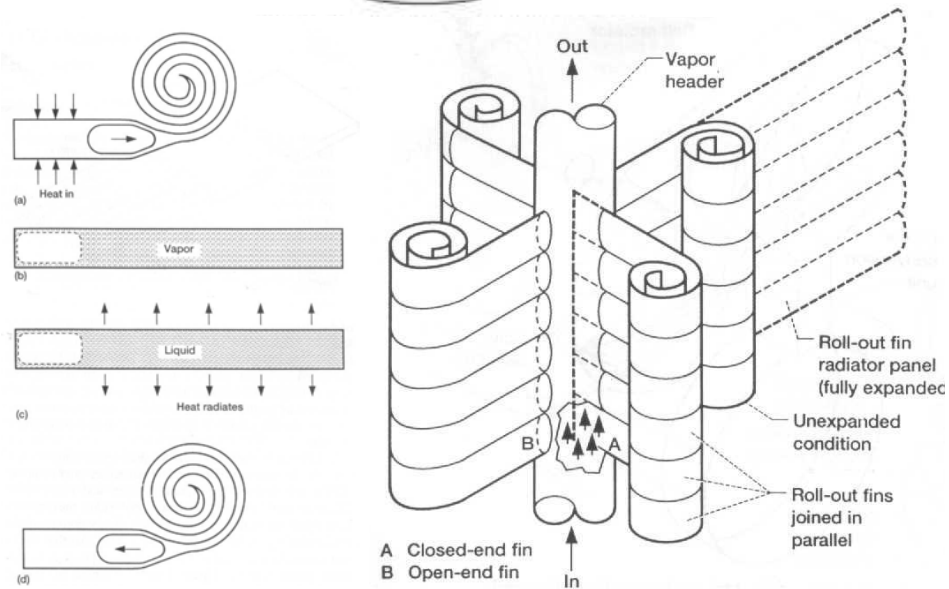
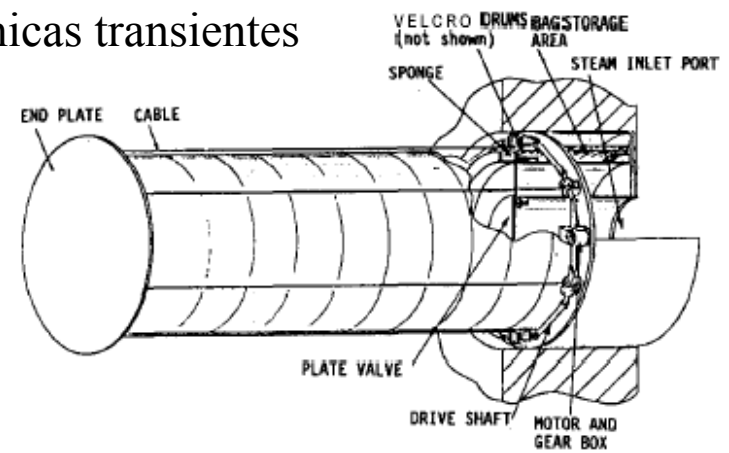
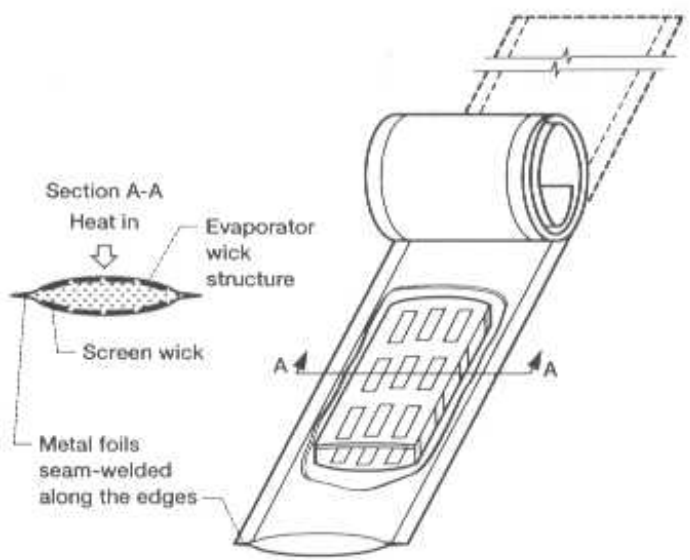


Primeiro satélite comercial
que usa radiadores retráteis
com LHP (HPs flexíveis ?).

Boeing 702 Expanded View

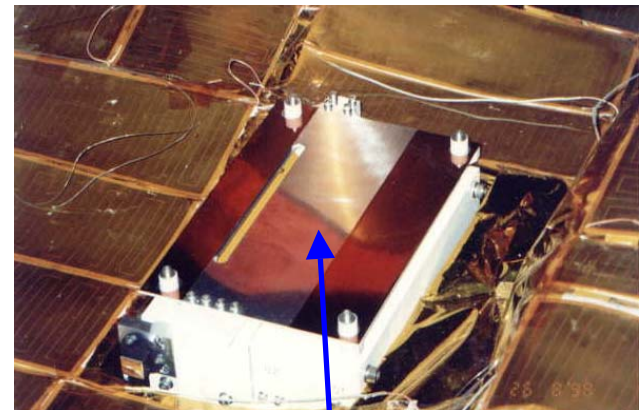
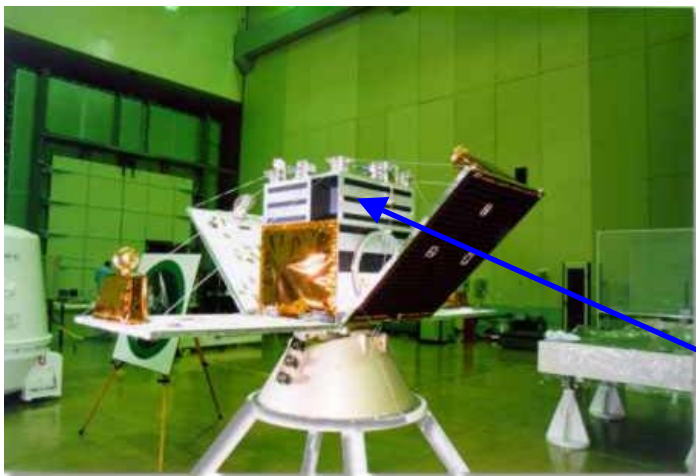


– Radiadores Infláveis: Dissipação de grandes cargas térmicas transientes



→ Radiadores Com Propriedades Termo-Ópticas Constantes

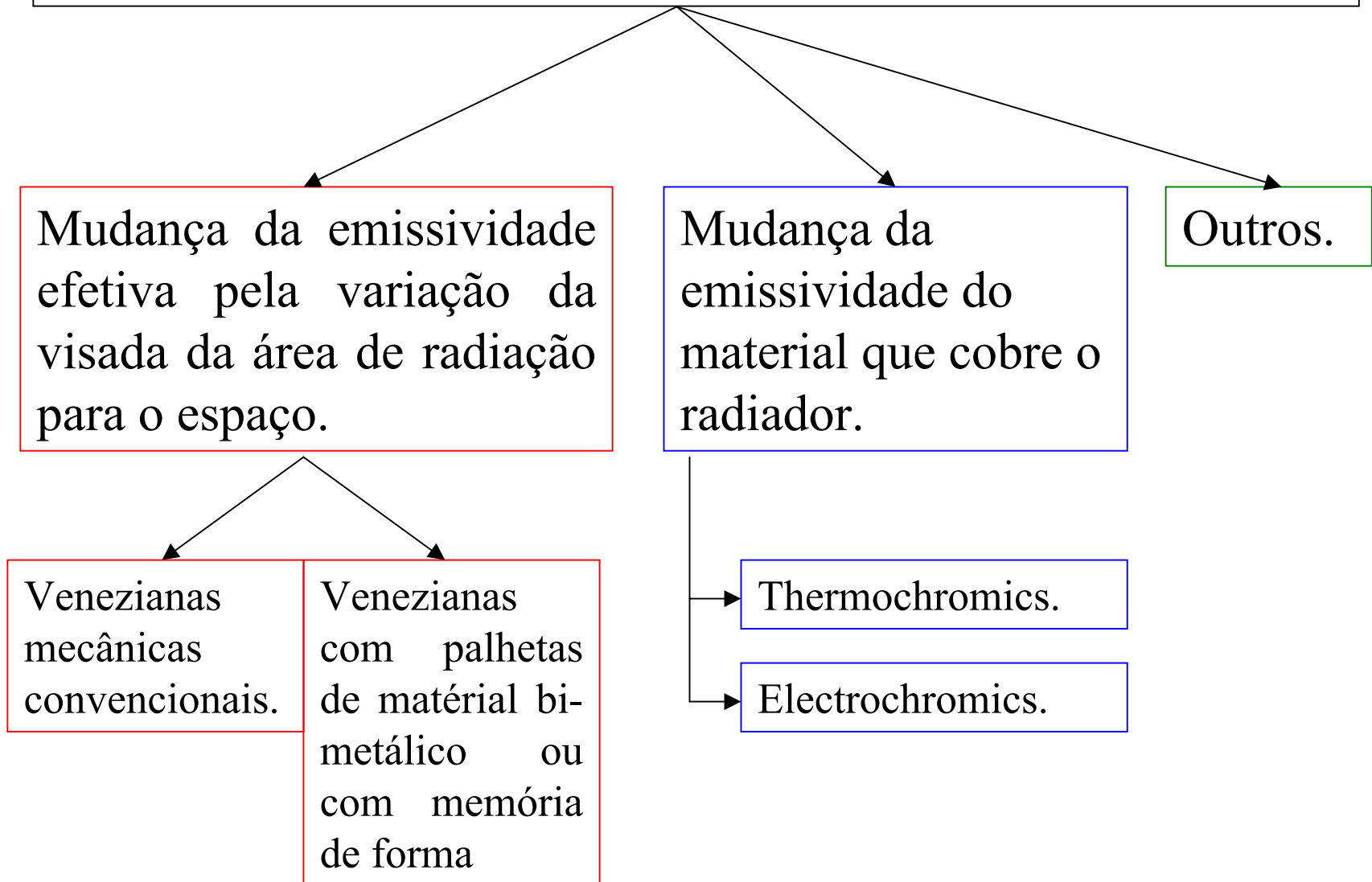
- Normalmente os radiadores são projetados com uma determinada relação α/ε que se manteria constante ao longo da vida útil do satélite (o valor desta relação só varia pela degradação das propriedades termo-ópticas).
- Diferentes coberturas podem ser usadas conjuntamente sobre a superfície de um radiador para obter-se uma determinada propriedade *efetiva*.



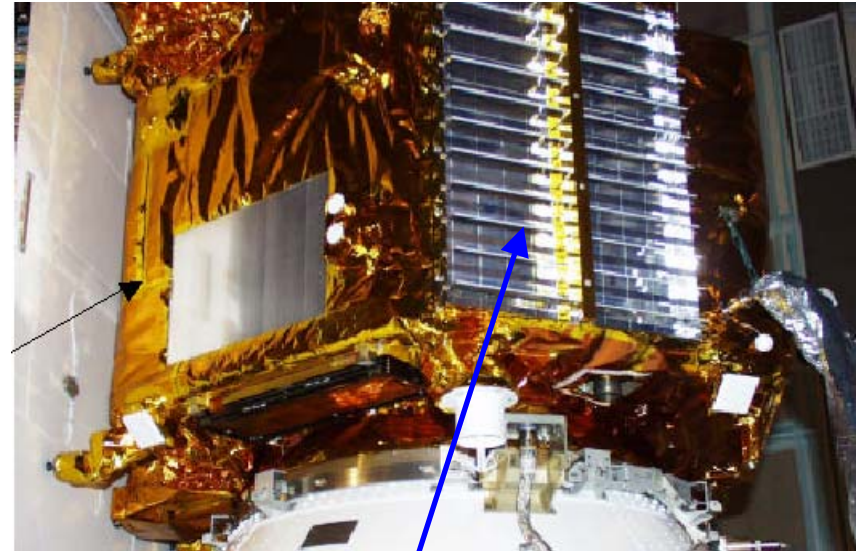
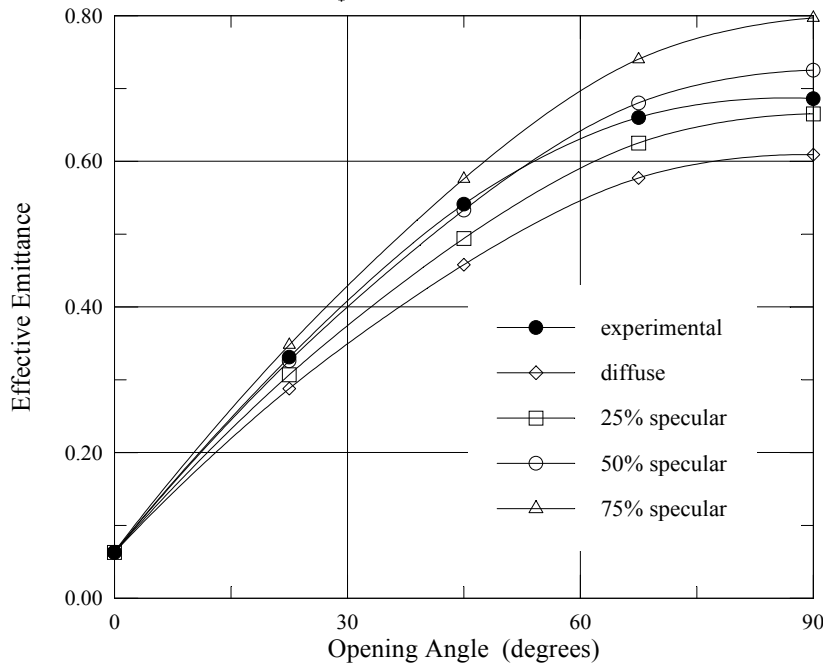
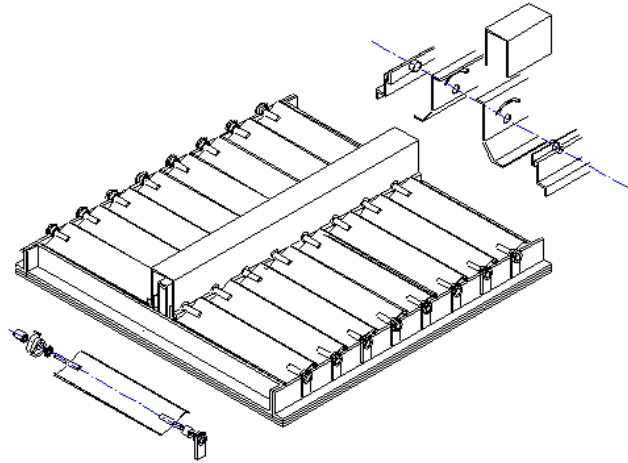
Radiador do WFI
CBERS - FM1

Radiadores com um
“mosaico” de coberturas

Radiadores com Propriedades termo-ópticas variáveis

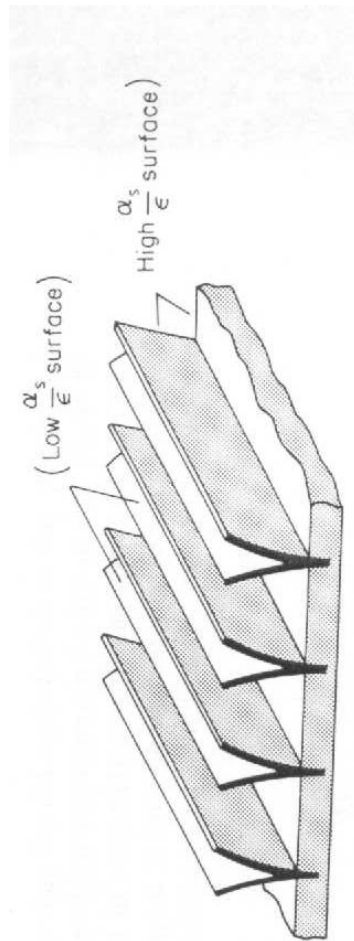


- Venezianas mecânicas tradicionais.

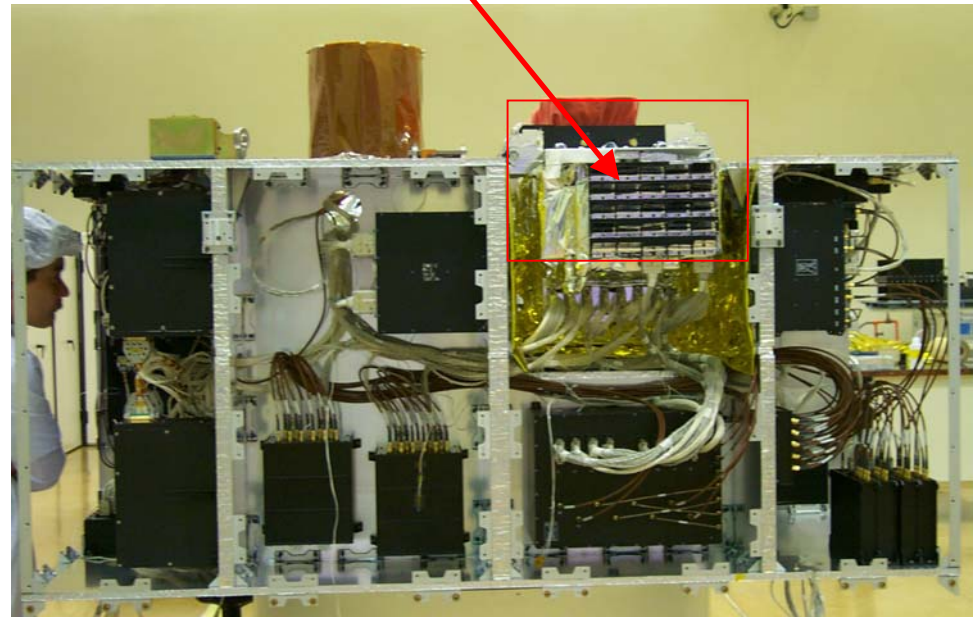


Venezianas sobre radiador do painel das baterias no satélite EO-1

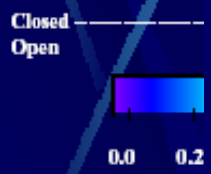
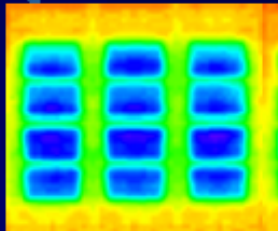
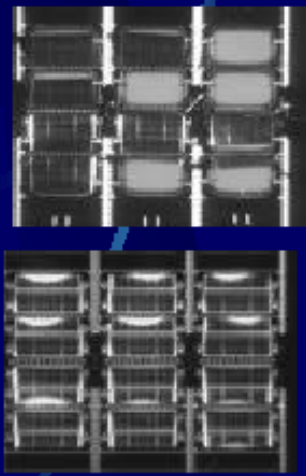
- Venezianas com palhetas em material bi-metálico ou de memória de forma .



Radiador lateral da câmera CCD
 CBERS - FM2



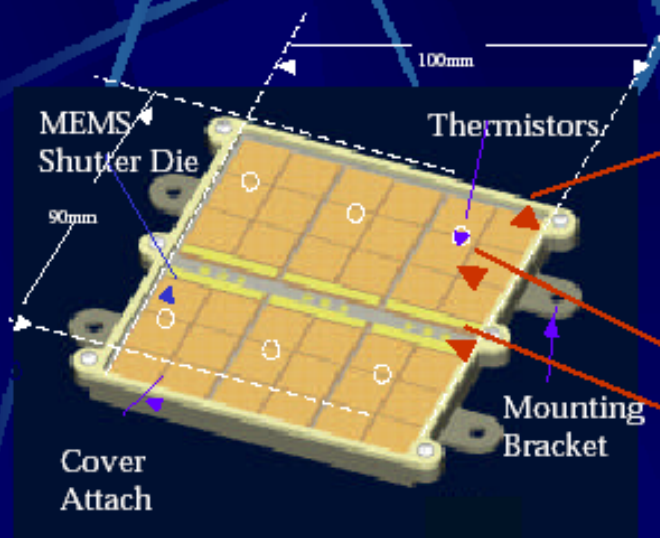
- Micro venezianas: milhares de micro-venezianas (6 - 150 μm) são acionadas eletrostaticamente (40 V).



Optical image of louvers with etched openings, with open louvers (top) and all closed (bottom).

Infrared images (states, effective em 0.88).

MEMS VEC Radiator - "Package"

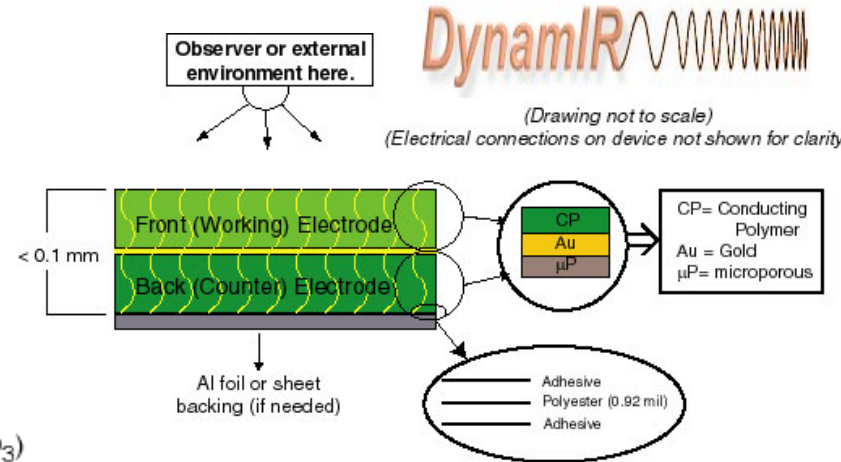
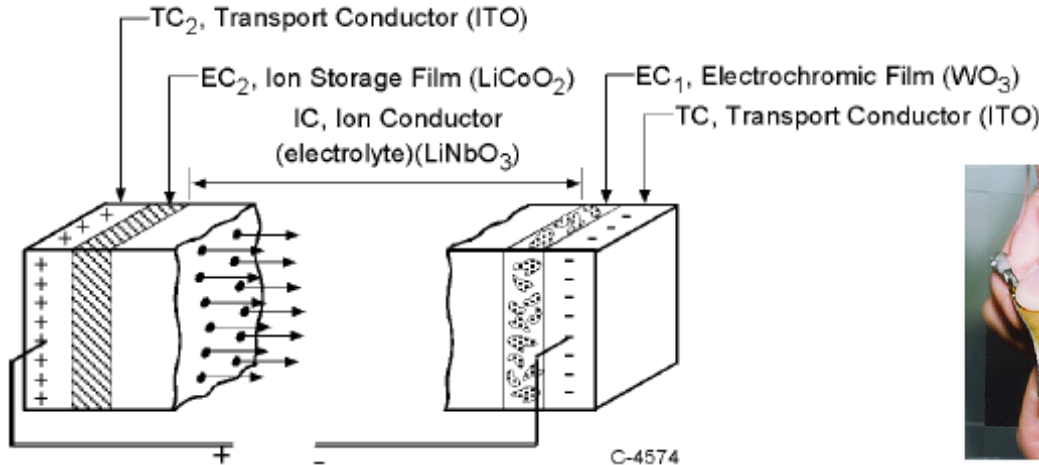


- Two 9cm x 10 cm Radiators, one on each Spacecraft
- Feed thru to back
- 36 Shutter Arrays, 12.65 mm x 13.03 mm, 72 Building Blocks each, entire area actuated, fixed w. Epoxy (Hysol IP 4402/4450)
- Temperature Sensors on back
- Wirebonds to Dies
- Heater 1.5 W on back
- Tradeoff Yield - Assembly

Experimento no satélite tecnológico ST5 a ser lançado em 2004.

• Electrochromics

- Determinados materiais (“compostos”) podem mudar sua transmissividade quando submetidos à uma diferença de potencial ($< 5 \text{ V}$).
- Mudança de propriedade óptica se dá por meio da aplicação de uma DDP transiente.
- Radiador pode ser construído depositando o material sobre uma superfície com alto ϵ .



(a) -0.8 V



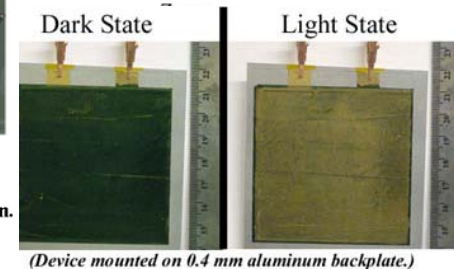
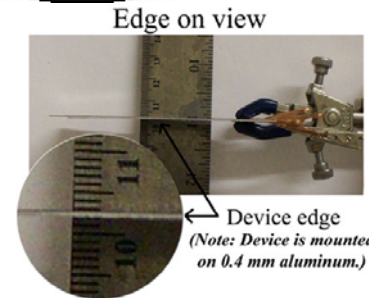
(b) 0.0 V



(c) +0.8 V

Bending/Flexing has no effect on device function.

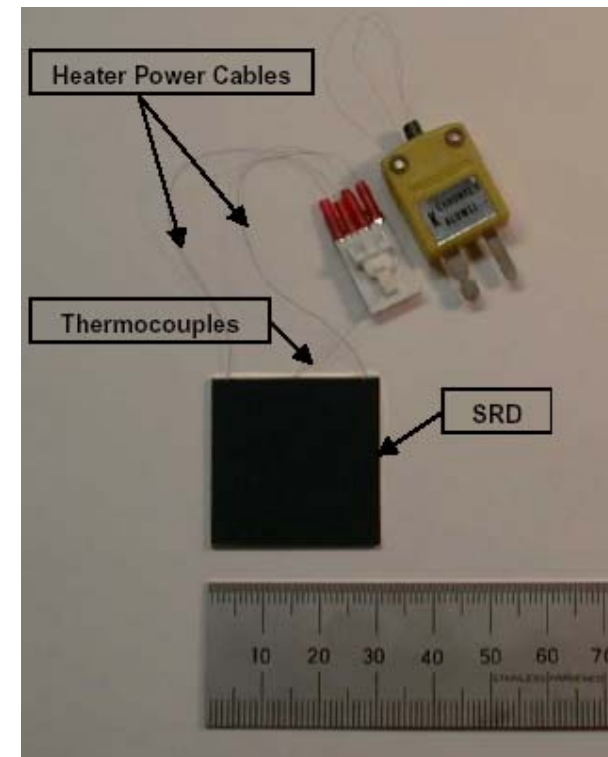
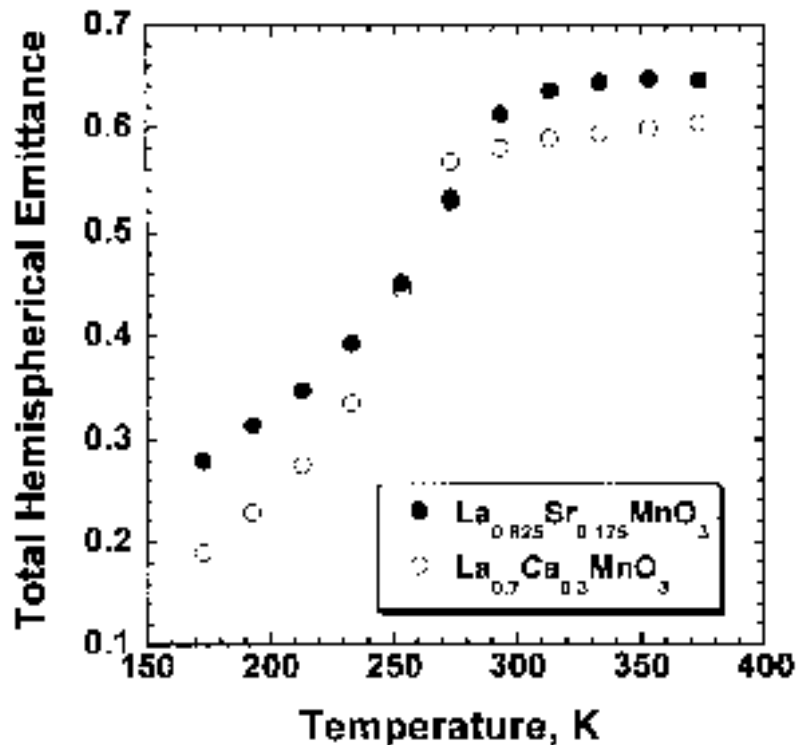
(All pictures are raw data and are not modified in any way.)



Experimento no satélite tecnológico ST5 a ser lançado em 2004.

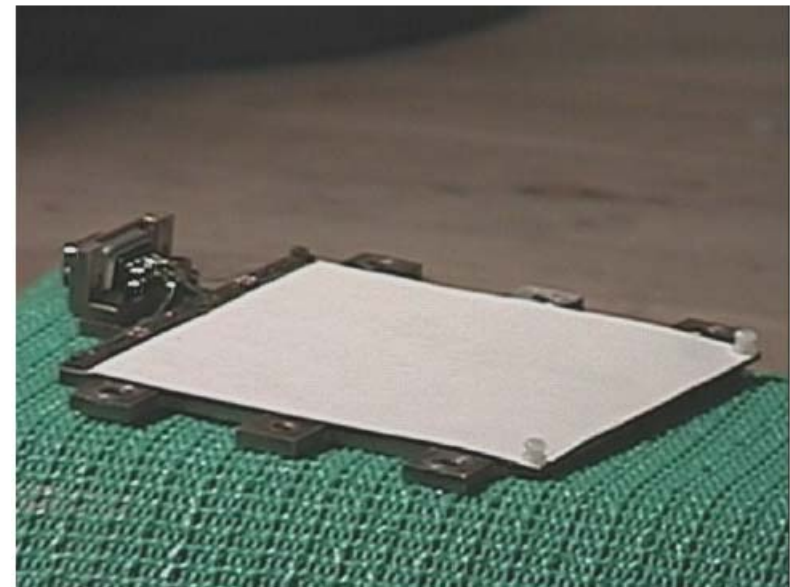
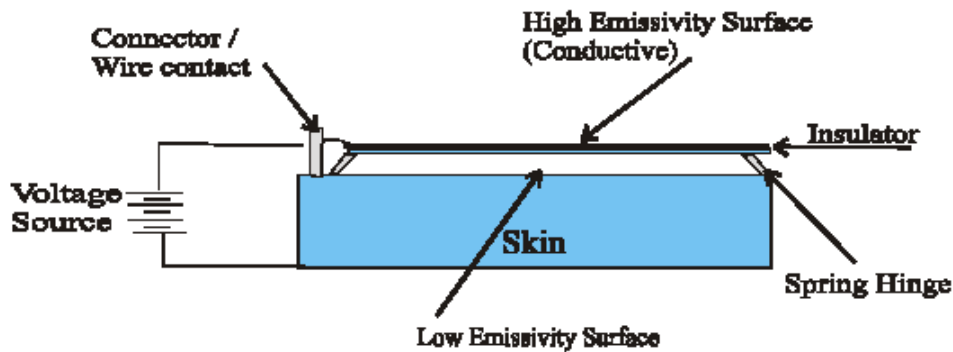
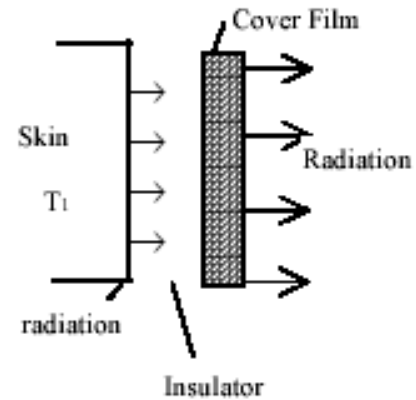
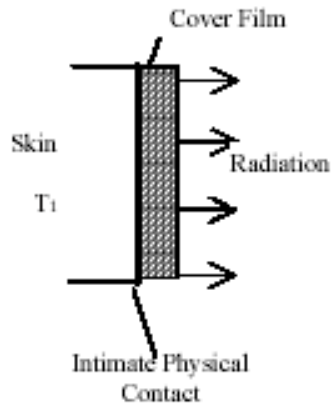
• Thermochromics

- Determinados materiais sofre uma mudança na propriedade termo-óptica com a temperatura.
- Radiador seria construído fixando diversas pastilhas deste material sobre sua superfície .
- Não há degradação das PTO devido à irradiação UV, por prótons ou elétrons.
- Problema: alto valor de α (0.84-0.9).



Smart Radiation Device

Radiador “eletrostático”: 200 - 500 V



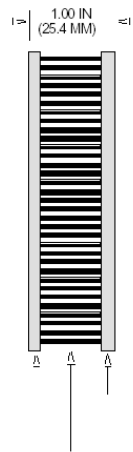
Experimento no satélite
 tecnológico ST5 a ser
 lançado em 2004.

→ Radiadores Carbono-Carbono

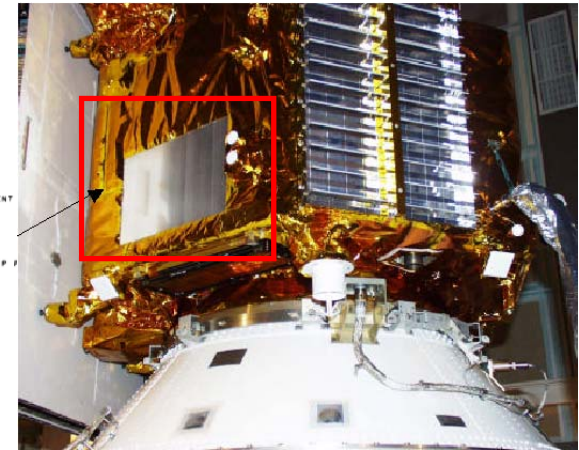
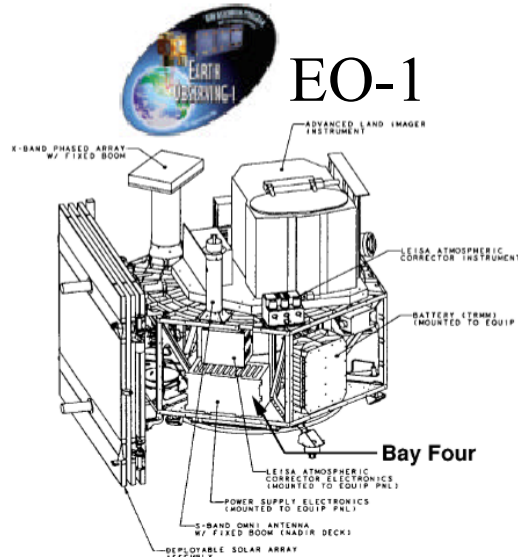
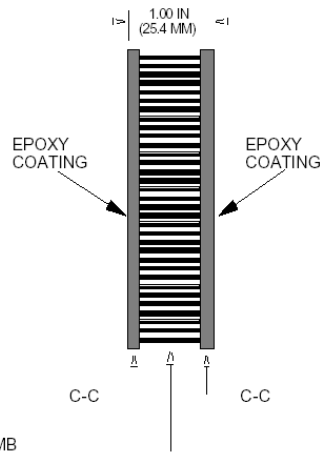
- Materiais C-C (fibra e matriz em Carbono) oferecem maior eficiência térmica, razão rigidez/massa, “tailorability” e estabilidade dimensional que o alumínio.



BASELINE



C-C RADIATOR



	Pre-Flight / Experimental	Flight Analysis
K (horizontal)	230 W/m-K	295 W/m-K
K (vertical)	230 W/m-K	208 W/m-K
K (z direction)	30 W/m-K	30 W/m-K

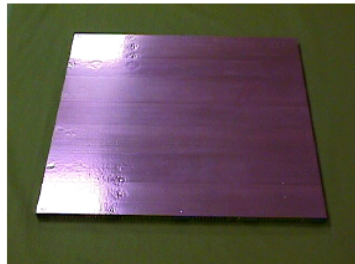


Figure 1.1

Carbon-Carbon Panel Internal Surface

Figure 1.2

Carbon-Carbon Panel External Surface

LESSONS LEARNED

- C-C Radiator was a success and proved that the technology can work to reduce Spacecraft weight
- C-C has a niche, especially for high temperatures
- C-C still needs further development (my opinion)
 - Reduction in fabrication time and cost - high conductivity “traditional” composites are more competitive
 - CTE Interface issues with heat pipes
- Redundancy a good idea - we flew the spare panel

- Radiador com face-sheets e Honeycomb de C-C.



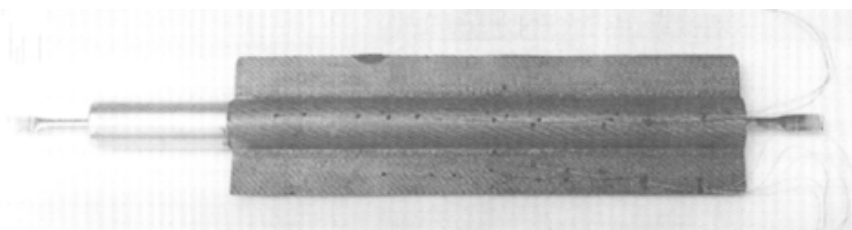
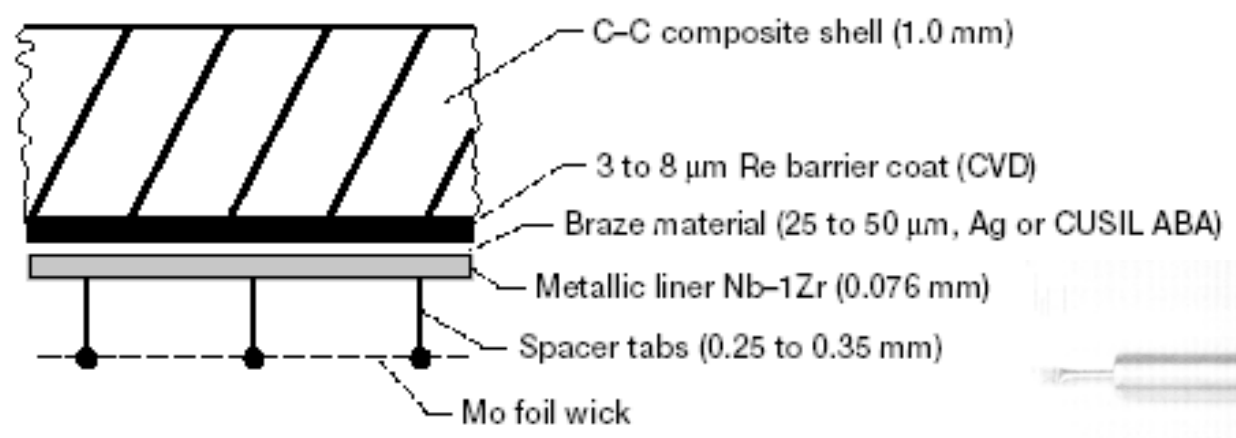
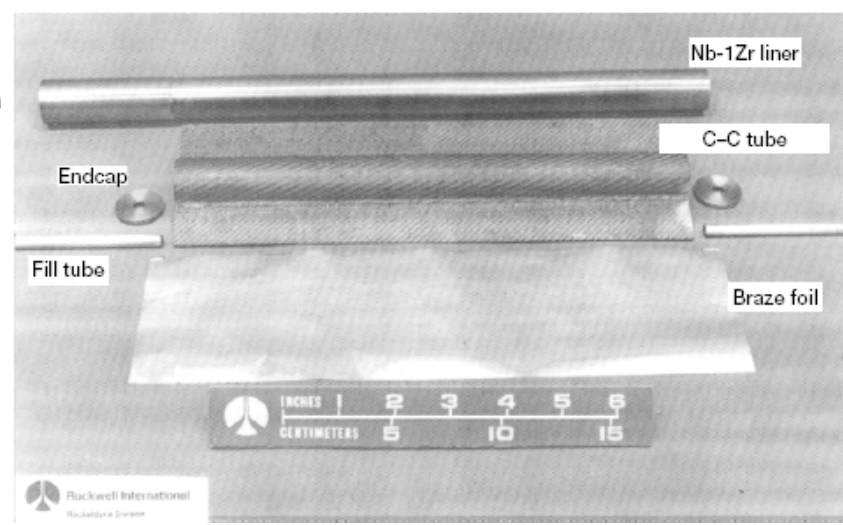
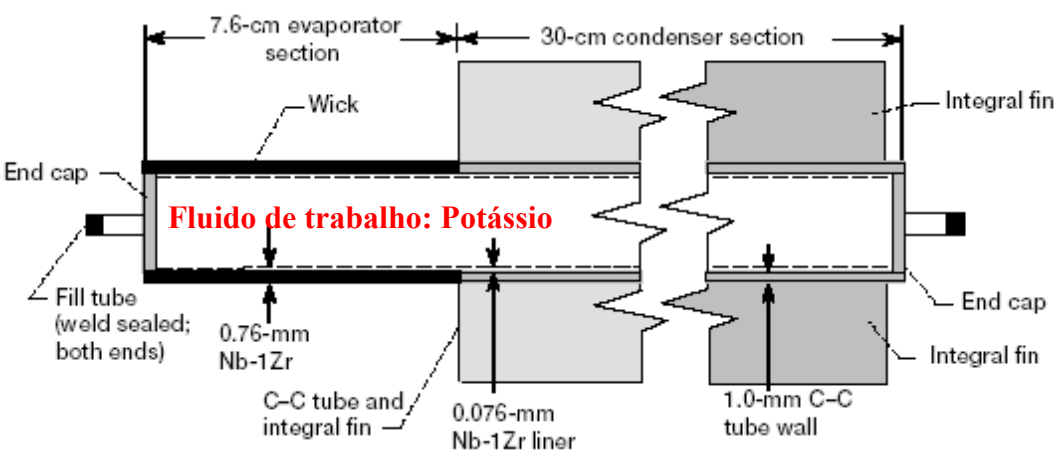
	Ultracor C-C H/C Panel	P-120 Facesheets Al. H/C	Aluminum Facesheets Al. H/C	Aluminum Plate
Thermal Conductivity (in plane) (W/mK)	350	275	180	180
Density (g/cc)	0.27	0.2	0.3	2.7
Specific Thermal Conductivity (W-cm ³ /mK-g)	1296	1375	600	66
Thermal Conductivity in Z-direction (W/mK)	65	20	10	180
Specific Thermal Conductivity (W-cm ³ /mK-g) In Z	241	100	33	66

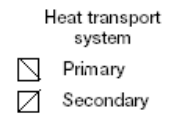
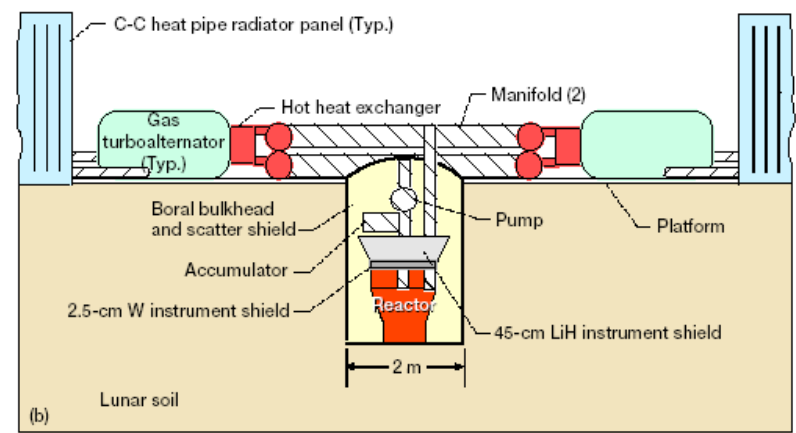
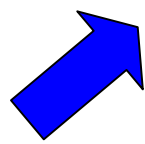
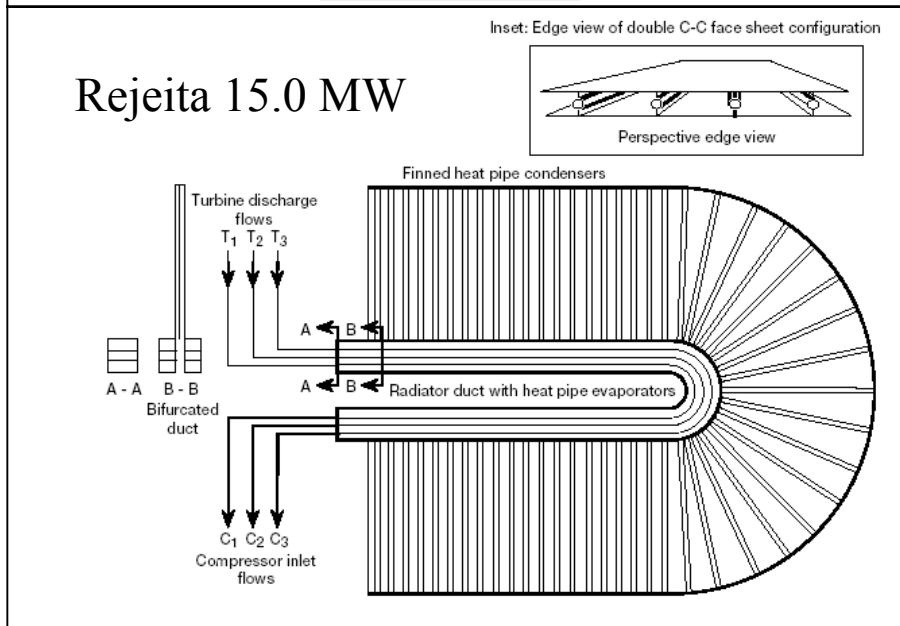
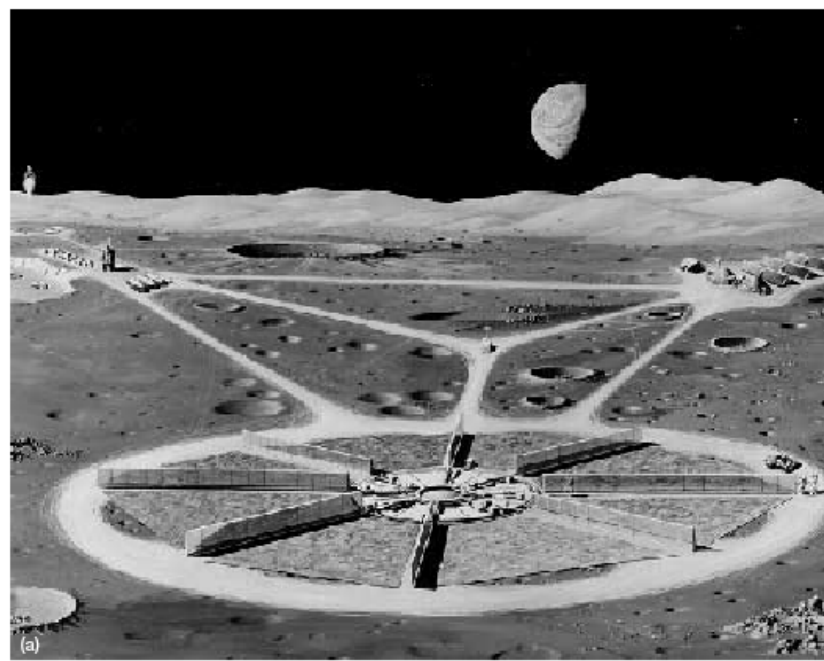
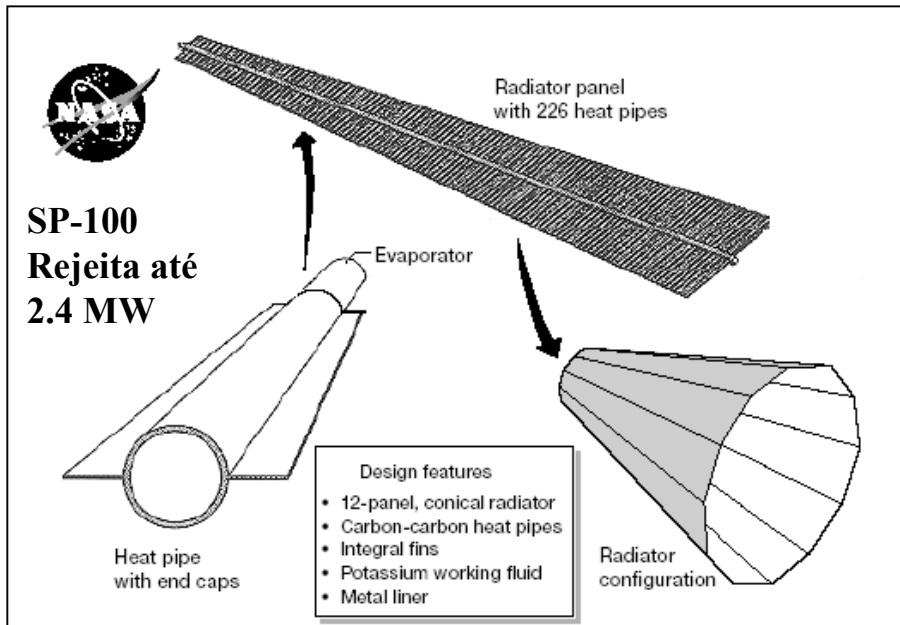
Dados do EO-1 facesheets CC - HC Al	Pre-Flight / Experimental	Flight Analysis
K (horizontal)	230 W/m-K	295 W/m-K
K (vertical)	230 W/m-K	208 W/m-K
K (z direction)	30 W/m-K	30 W/m-K

- Radiador C-C com HPs (C-C) para sistemas com alta dissipação de potência.

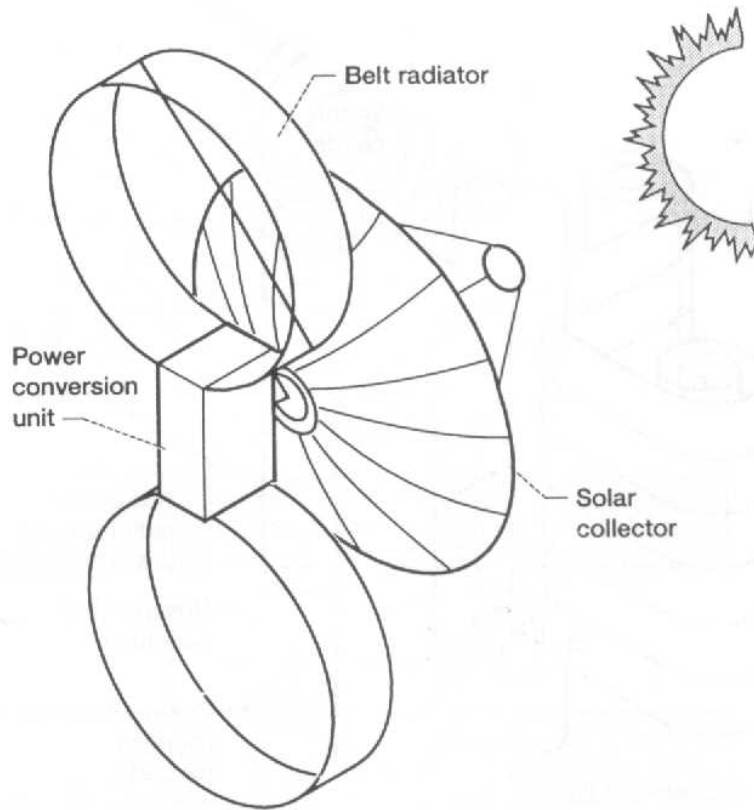


Glenn Research Center,

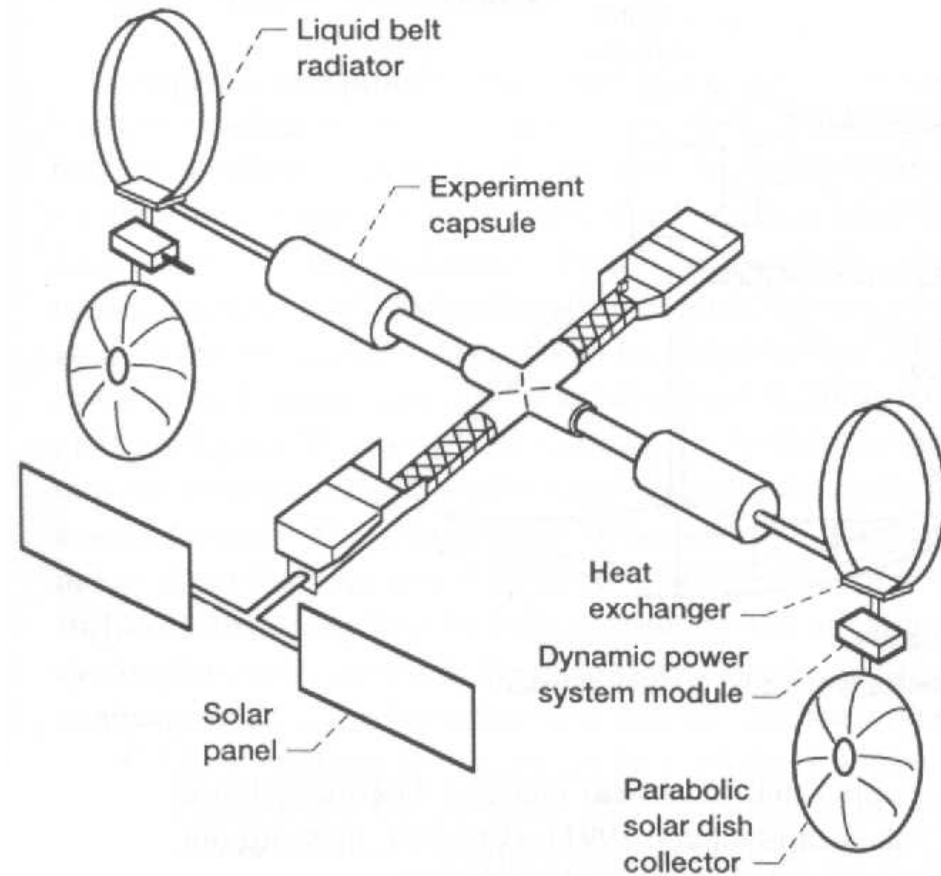




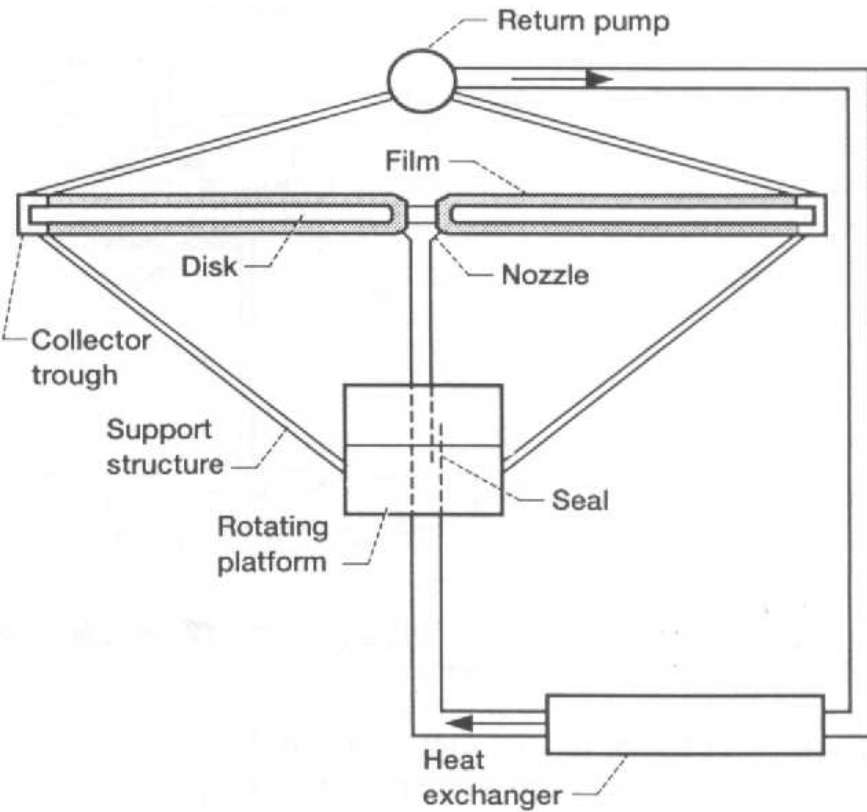
→ Outras Concepções Avançadas Para Sistemas de Alta Dissipação



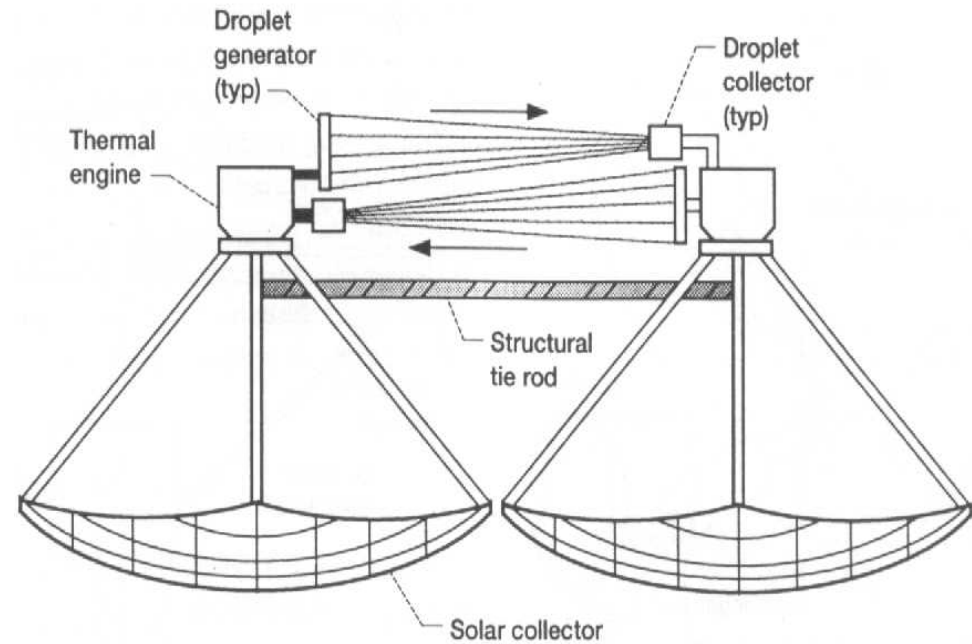
Moving-belt radiator



Liquid-belt radiator

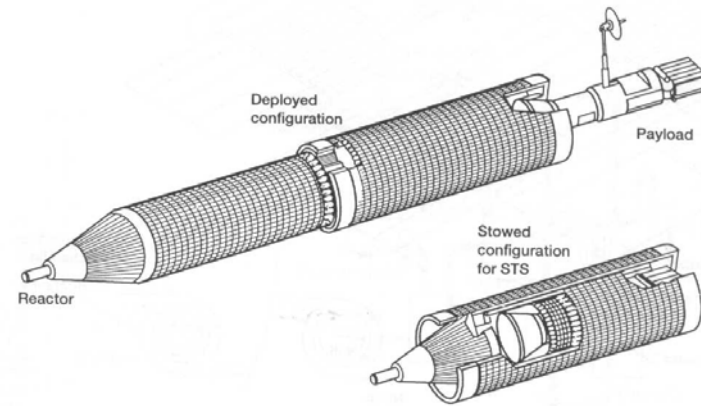
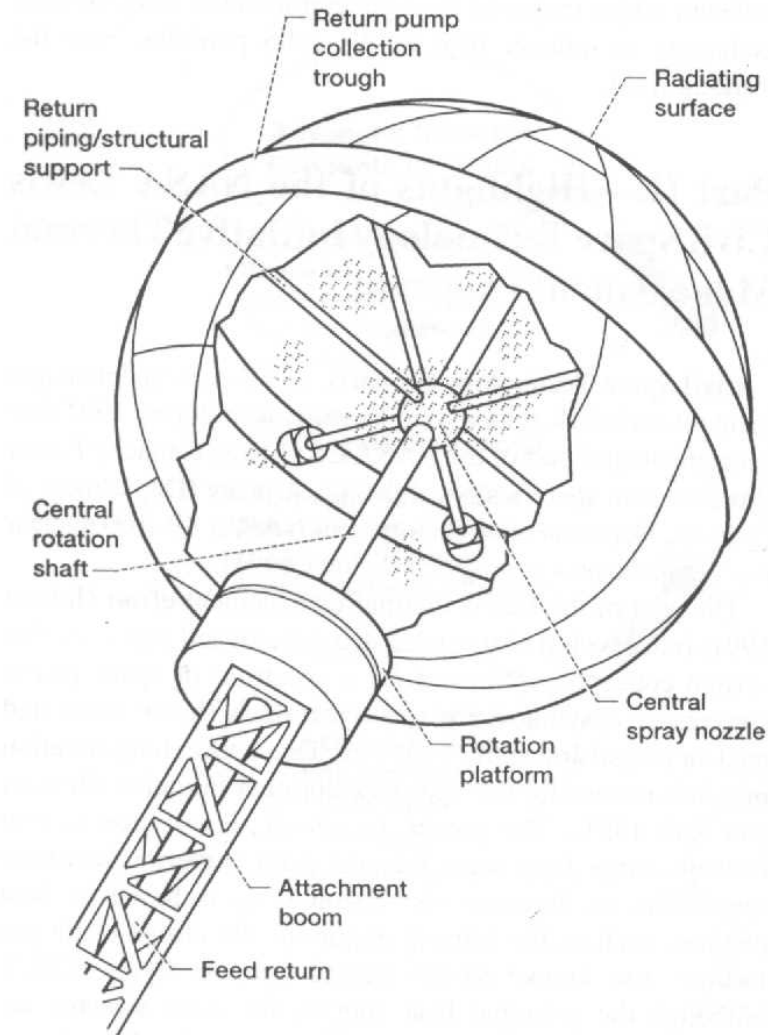


Rotating film radiator

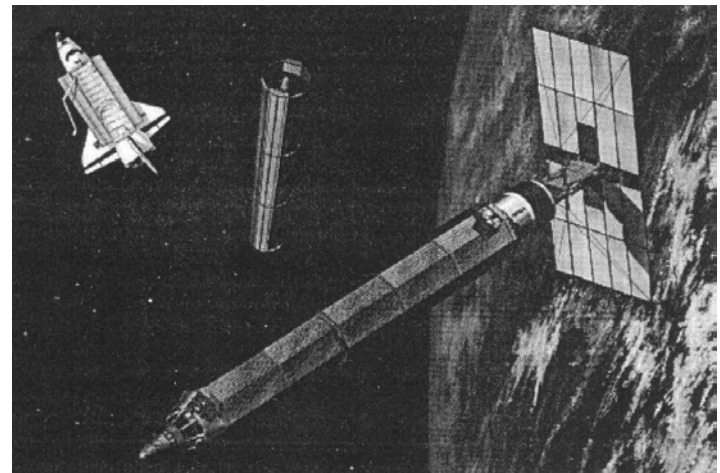


Liquid droplet radiator

Conceito similar, mas com partículas sólidas: Curie Point Radiator.



Telescoping radiator (K HPs)



Folding panel radiator (Li/NaK loops)

Rotating bubble-membrane radiator

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